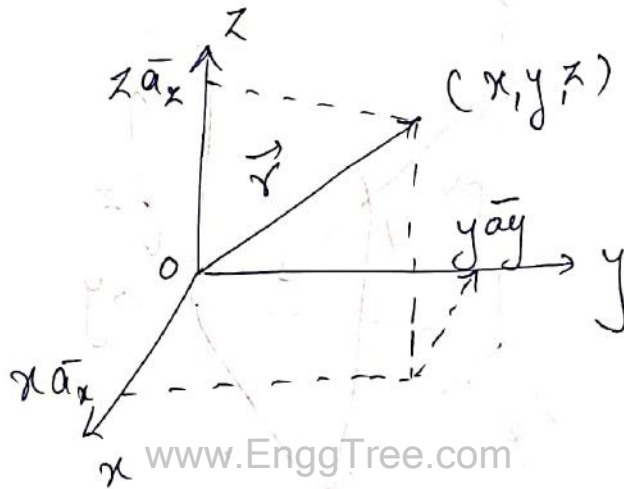


## ELECTROSTATICS - I

1.) Coordinate Systems :-

→ Simplex way of representing vectors.

1.1 The Cartesian Co-ordinate Systems:-



$$r = \bar{a}_x x + \bar{a}_y y + \bar{a}_z z$$

where  $\bar{a}_x, \bar{a}_y, \bar{a}_z$  are unit-vectors.

Unit vector → in a given direction is a vector in that direction divided by magnitude, It is given by

$$a_r = \frac{x\bar{a}_x + y\bar{a}_y + z\bar{a}_z}{\sqrt{x^2 + y^2 + z^2}}$$

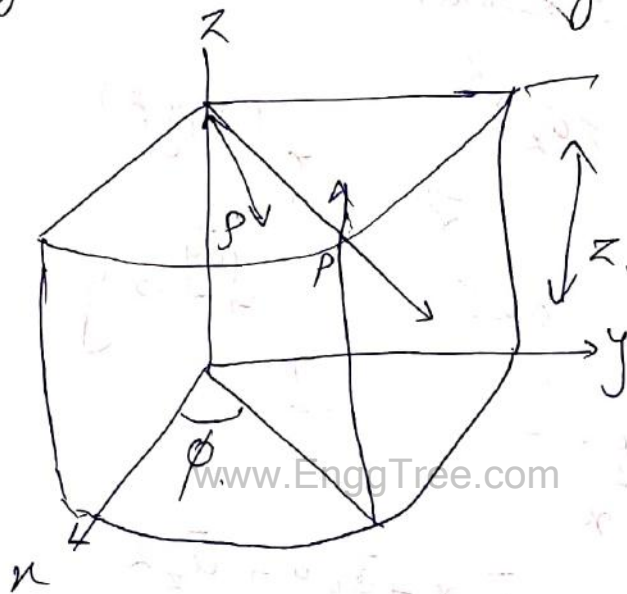
→ The differential length  $dl$  from P to Q is a diagonal is given by,

$$dl = \sqrt{(dx)^2 + (dy)^2 + (dz)^2}$$

The differential area  $ds = dx dy$   
 $= dy dz$   
 $= dz dx.$

differential Volume  $dV = dx dy dz.$

1.2. Cylindrical Co-ordinate System :-



→ Consider any point as the intersection of three mutually perpendicular surfaces.

→ a cylinder ( $\rho$ ), a plane ( $\phi$ ) and another plane ( $z$ )

→ for a parallelepiped has the sides  $d\rho$ ,  $\rho d\phi$  and  $dz$ .

$$dl = \sqrt{(d\rho + \rho d\phi)^2 + (dz)^2}$$

$$ds = \rho d\rho d\phi = d\rho dz = \rho d\phi dz.$$

→ In this system consider any point of intersection of the spherical surface (radius  $r$ ) & conical surface ( $\theta$ , angle b/w  $r$  &  $z$ ) & a plane surface ( $\phi = \text{constant}$ ), The co-ordinates are  $r, \theta, \phi$ .

$$\text{differential length } dl = \sqrt{dr^2 + (rd\theta)^2 + (r\sin\theta d\phi)^2}$$

$$\begin{aligned} ds &= dr \cdot r d\theta = r dr d\theta \\ &= dr r \sin\theta d\phi = r \sin\theta d\phi dr \\ &= r d\theta \cdot r \sin\theta d\phi \\ &= r^2 \sin^2\theta d\theta d\phi \end{aligned}$$

### Conversion

(i) Cartesian to cylindrical

$$\begin{array}{l} x \\ y \\ z \end{array} \quad \begin{array}{l} \rho = \sqrt{x^2 + y^2} \\ \phi = \tan^{-1}(y/x) \\ z = z \end{array}$$

(ii) Cylindrical to Cartesian.

$$\begin{array}{l} \rho \\ \phi \\ z \end{array}$$

$$\begin{array}{l} x = \rho \cos\phi \\ y = \rho \sin\phi \\ z = z \end{array}$$



(iii) Cartesian to spherical

$$\begin{aligned}x & r = \sqrt{x^2 + y^2 + z^2} \\y & \theta = \cos^{-1} \left( \frac{z}{\sqrt{x^2 + y^2 + z^2}} \right) \\z & \phi = \tan^{-1} (y/x).\end{aligned}$$

1.4. Vector fields: -

→ The Quantity that contains direction.

→ for vector multiplication take

$$|A \times B| = AB \sin \theta.$$

$$A \times B = \begin{vmatrix} a_x & a_y & a_z \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

→ Co-efficients of vectors in each direction.

(i) Gradient: -

$$\nabla V = \frac{\partial V}{\partial x} \bar{a}_x + \frac{\partial V}{\partial y} \bar{a}_y + \frac{\partial V}{\partial z} \bar{a}_z$$

This operation is called gradient

$$\boxed{\nabla V = \text{grad } V}$$



(ii) Divergence [www.EnggTree.com](http://www.EnggTree.com)

$$\nabla \cdot A = \lim_{V \rightarrow 0} \frac{1}{V} \oint A \cdot \hat{n} ds.$$

Can be expressed as

$$\nabla \cdot A = \left[ \bar{a}_x \frac{\partial}{\partial x} + \bar{a}_y \frac{\partial}{\partial y} + \bar{a}_z \frac{\partial}{\partial z} \right]$$

$$\left[ a_x A_x + a_y A_y + a_z A_z \right].$$

$$\text{So } \therefore \nabla \cdot A = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}.$$

$$\boxed{\nabla \cdot A = \text{div } A}$$

(iii) Curl :- [www.EnggTree.com](http://www.EnggTree.com)

$$\text{Curl } A = \nabla \times A = \begin{vmatrix} a_x & a_y & a_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$$

1.5. Theorems & Applications :-

1) Divergence theorem :-

→ The volume integral of the divergence of a vector field over a volume is equal to the surface integral of the normal component of this volume bounding the volume.

$$\iiint_V \nabla \cdot A \, dV = \oint_S A \cdot ds.$$

→ for the proof ref. EMT (by Dhanrajayan)  
page 1.17.

2) Stokes theorem:-

→ The line integral of a vector around a closed path is equal to the surface integral of the normal component of its curl over any closed surface.

$$\oint H \cdot dl = \iint_S \nabla \times H \cdot ds.$$

Note:- proof ref. text EMT page no 1.19.

Applications:-

Exp: Using divergence theorem, evaluate

$$\iint_S \vec{F} \cdot nds \text{ where } \vec{F} = 2xy \hat{i} + y^2 \hat{j} + 4yz \hat{k}$$

and  $S$  is the surface of the cube bounded

by  $x=0, x=1, y=0, y=1$  and  $z=0, z=1$ .

Hint:- find using divergence theorem.

Expt 2. Check the validity of the divergence theorem considering the field

$$D = 2xy \hat{a}_x + x^2 \hat{a}_y \text{ e/m}^2 \text{ and}$$

rectangular parallelepiped formed by the planes  $x=0, x=1; y=0, y=2$  and  $z=0, z=3$ .

Hint :- use Divergence theorem and

Solve of both sides.

Expt 3. If  $F = x^2 \hat{a}_x + y^2 \hat{a}_y + z^2 \hat{a}_z$ , then find divergence of  $F$  & curl of  $F$ .

Hint:  $\text{Div } F = \nabla \cdot F$

$$\text{Curl } F = \nabla \times F.$$

Expt: Solve that  $\vec{H} = x^2 \hat{a}_x + y^2 \hat{a}_y + z^2 \hat{a}_z$  is a conservative field.

Hint :- if  $\vec{H}$  is conservative field if  $\text{Curl } \vec{H} = 0$ .



## 1.6 Coulomb's Law EnggTree.com

→ force b/w two small objects separated by a distance which is large compared to their size is proportional to the charge on each & inversely proportional to the square of distance b/w them.

$$F \propto \frac{Q_1 Q_2}{r^2}$$

$$F = k \frac{Q_1 Q_2}{r^2}$$

$$k = \frac{1}{4\pi\epsilon_0} = 9 \times 10^9$$

$\epsilon_0$  → Absolute permittivity in free space  
→  $8.85 \times 10^{-12} \text{ F/m}$

$\epsilon$  → permittivity of medium

$\epsilon_r$  → relative permittivity

$$\boxed{\epsilon_0 = \frac{\epsilon}{\epsilon_r}}$$

1.7 Continuous charge Distribution:-

(i) Linear charge density:-

→ total charge distributed over a line or curve.

$$\rho_l = \frac{Q}{l} \text{ Coulomb/m.}$$

(ii) Surface charge density:-

→ Total charge distributed over a surface.

$$\rho_s = \frac{Q}{S} = \frac{Q}{A} \rightarrow C/m^2$$

(iii) Volume charge density:-

→ Total charge distributed over a volume.

$$\rho_v = \frac{Q}{V} \rightarrow C/m^3.$$

1.8. Electric field Intensity:-

→ Electric force per unit charge

$$E = F/q.$$

According to Coulomb's law

$$F = \frac{Q_1 Q_2}{4\pi\epsilon_0 r^2}$$

$$E = F/q = \frac{Q}{4\pi\epsilon_0 r^2} \quad \underline{\underline{N/Coulomb.}}$$

## 1.9. Gauss Law & its Applications:-

Gauss law :-

→ Electric flux passing through any closed surface is equal to the total charge enclosed by the surface.



→ Consider a small element of area  $ds$  in a plane surface having a charge  $Q$  &  $P$  be a point in the element → electric flux density  $D$  will have a value  $D_s$ . → makes an angle  $\theta$ .

$$\begin{aligned} d\phi &= D_s \text{ normal} \cdot ds \\ &= D_s \cos\theta \cdot ds. \end{aligned}$$

$$d\phi = D_s \cdot ds \quad (\text{dot-product}).$$

→ total flux passing through the closed surface is given by



$$\mathcal{N} = \int d\mathcal{N} = \oint \mathbf{D}_s \cdot d\mathbf{s}.$$

$$\mathcal{N} = Q.$$

System of Volume charge density

$$\mathcal{N} = \int_V \rho_r \, dV = Q.$$

Note: - proof - refer EMT page 2.2.

Electric flux :- ( $\mathcal{N}$ )

→ Electric flux is equal to charge it-self.

$$\mathcal{N} = Q.$$

Electric flux density ( $D$ )

→ electric flux per unit area.

$$D = \frac{Q}{A}.$$

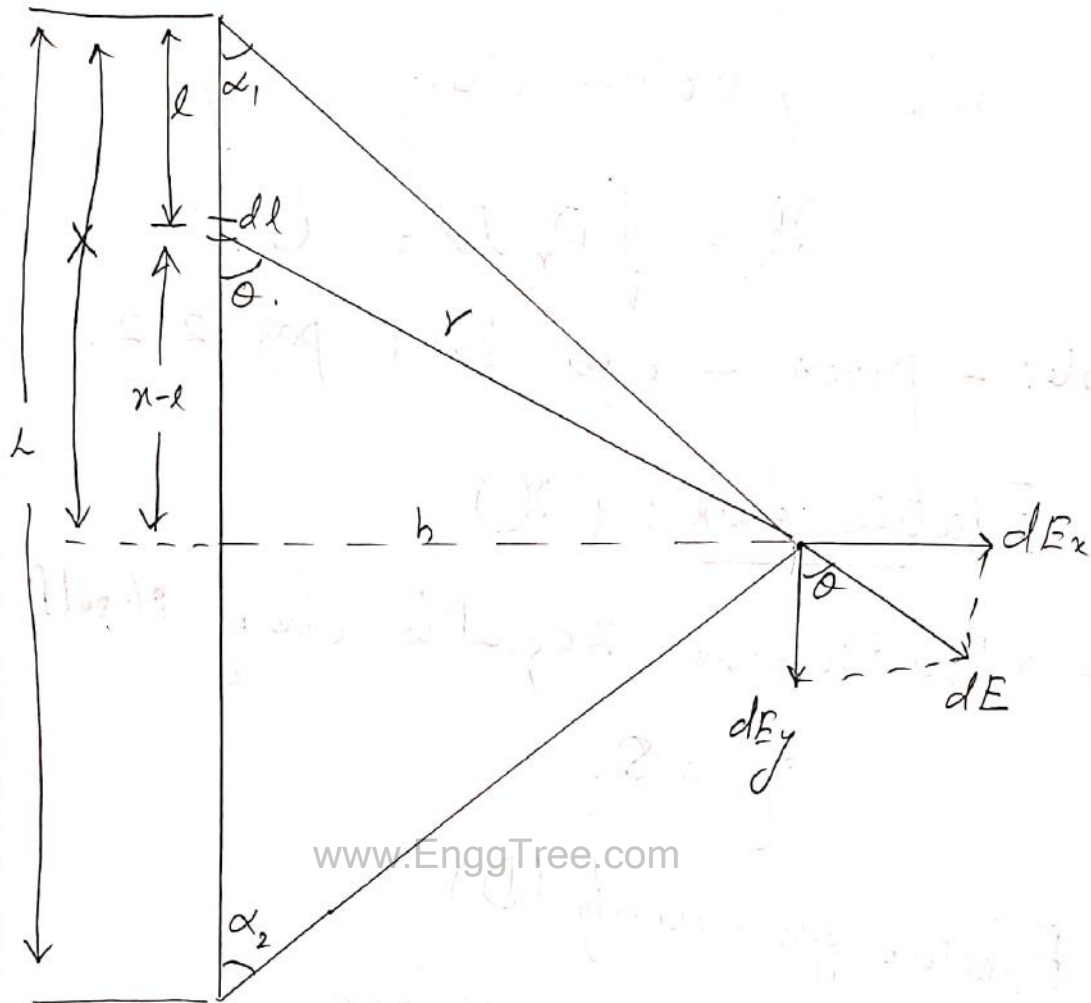
$$A = 4\pi r^2.$$

$$D = \frac{Q}{4\pi r^2}$$

$$\text{but } E = \frac{Q}{4\pi \epsilon_0 r^2}$$

$$\boxed{D = \epsilon_0 E}$$

1.10. Field line of charge :-



www.EnggTree.com

- Consider a uniform charged line of length 'L' whose linear charge density is  $\rho_L$  C/m.
- Consider a small element 'dl' at a distance 'x' from one end of line.
- point 'P' is taken from distance 'r' from 'dl'.

The electric field at point P due to charged element  $\rho_L dl$  is

$$dE = \frac{\rho_L dl}{4\pi\epsilon_0 r^2}$$

→ The x & y components of electric field  
 $dE$  is given by

$$dE_x = dE \sin \theta$$

$$dE_y = dE \cos \theta$$

Then  $dE_x = \frac{\rho_e dl \sin \theta}{4\pi \epsilon_0 r^2}$

From the figure

$$x - l = h \cot \theta$$

$$-dl = -h \operatorname{cosec}^2 \theta d\theta$$

and  $h/r = \sin \theta$ ,  $r = h \operatorname{cosec} \theta$

$$dE_x = \frac{\rho_e dl \sin \theta}{4\pi \epsilon_0 h}$$

The electric field  $E_x$  due to entire length of  
 line of charge is given by

$$E_x = \int_{\alpha_1}^{\alpha_2} \frac{\rho_e \sin \theta d\theta}{4\pi \epsilon_0 h}$$

$$= \frac{\rho_e}{4\pi \epsilon_0 h} \int_{\alpha_1}^{\alpha_2} \sin \theta d\theta$$

$$= \frac{\rho_e}{4\pi \epsilon_0 h} [-\cos \theta] = \frac{\rho_e}{4\pi \epsilon_0 h} [\cos \alpha_1 + \cos \alpha_2]$$



11] for  $E_y$  EnggTree.com

$$E_y = \frac{\rho_l}{4\pi\epsilon_0 h} [\sin\alpha_2 - \sin\alpha_1]$$

Case 1: if the point P is at bisector of a line

then  $\alpha_1 = \alpha_2 = \alpha$

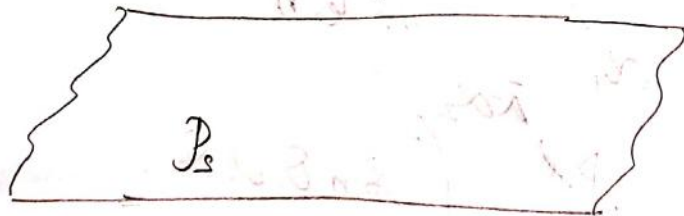
then  $E_y = 0$ , so  $E = \frac{\rho_l}{2\pi\epsilon_0 h} \cos\alpha$ .

Case 2: if the line infinitely long  $\alpha = 0$

$E_y = 0$   $E$  becomes  $E_x$

$$E = \frac{\rho_l}{2\pi\epsilon_0 h}$$

1.11. Electric field Intensity at a point due to charged circular Disc / infinite plane sheet of charge



→ Consider an infinite plane sheet which is uniformly charged with charged density of  $\rho_s$   $C/m^2$

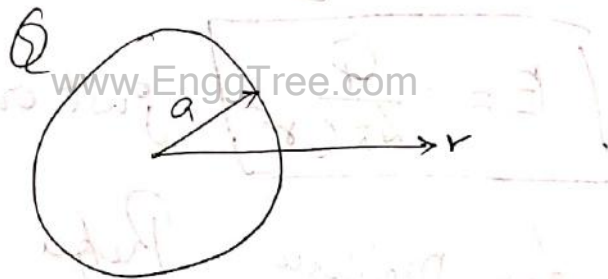
→ The field intensity at any point 'P' due to plane sheet of charge is

$$E = \frac{\rho_s}{2\epsilon} (1 - \cos \alpha)$$

$$E = \frac{\rho_s}{2\epsilon} \quad [\because \alpha = 90^\circ]$$

1.12 Electric field intensity due to shell of charge:-

→ Let positive charge is uniformly distributed over a spherical surface of radius as shown in figure.



→ by Applying Gauss law inside the shell, the integral of flux density  $D$  over a spherical surface is zero as no charge enclosed by the surface.

$$\oint D \cdot ds = 0 \quad r < a.$$

$$E \oint ds = 0$$
$$E = 0 \quad r < a. \quad (\text{Inside the shell.})$$

EnggTree.com  
→ Applying Gauss law just outside the shell,  
the  $\oint$  Integral of flux density  $D$  over a  
spherical surface is the charge of shell.

$$\oint_S D \cdot ds = Q$$

$$\epsilon \oint_S E \cdot ds = Q$$

$$\oint_S E \cdot ds = \frac{Q}{\epsilon}$$

$$E (4\pi r^2) = \frac{Q}{\epsilon}$$

$$\boxed{E = \frac{Q}{4\pi\epsilon r^2}} \text{ just outside the shell.}$$

Note: for problems Refer EMT by

Dananjayan — page — 1.20 to 1.35.



2.1 Electric potential EnggTree.com

→ Consider a uniform Electric field 'E' & a unit positive 'q'.

→ force with which unit test charge is moved from one point to another due to electric field

$$F = qE$$

→ The work done in moving unit positive charge from one point to another in an electric field is called potential Difference (V)

$$W = - \int_{r_1}^{r_2} qE \cdot dr$$

$$W = -q \int_{r_1}^{r_2} E \cdot dr$$

but

$$V = \frac{W}{q} = - \int_{r_1}^{r_2} E \cdot dr \quad \text{J/C}$$

But  $E = \frac{Q}{4\pi\epsilon_0 r^2}$ , So  $V = - \frac{Q}{4\pi\epsilon_0} \int_{r_1}^{r_2} \frac{1}{r^2} dr$

$$V = - \frac{Q}{4\pi\epsilon_0} \left[ \frac{1}{r} \right]_{r_1}^{r_2}$$

$$V = \frac{Q}{4\pi\epsilon_0} \left[ \frac{1}{r_1} - \frac{1}{r_2} \right] \text{ Volt. or}$$

EnggTree.com  
Electric potential is defined as work done in moving unit positive charge from infinity to a given point in Electric field.

$$V = \frac{Q}{4\pi\epsilon_0 r} \text{ Volt.}$$

→ In a conservative field

$$\oint E \cdot dr = 0.$$

Relation b/w Electric field & potential:-

→ In two points, work done will be

$$dW = dV = -E \cdot dr$$

→ Since scalar potential  $V$  is a function of  $x, y, z$ , above equation can be written as

$$\frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz = -E \cdot dr.$$

This can be re-written as,

$$\left[ \vec{a}_x \frac{\partial V}{\partial x} + \vec{a}_y \frac{\partial V}{\partial y} + \vec{a}_z \frac{\partial V}{\partial z} \right] \cdot \left[ \vec{a}_x dx + \vec{a}_y dy + \vec{a}_z dz \right]$$

$$= -E \cdot dr.$$

$$\nabla V \cdot dr = -E \cdot dr$$

$$\boxed{E = -\nabla V}$$



→ Conduction properties can be explained on the basis of electrons having energies in the Valance & Conduction bands.

→ If the Valance band merges smoothly into a Conduction band — resulting in electron flow — called a Solid metallic Conductor — no forbidden energy gap.

→ The forbidden energy gap b/w Valance and Conduction band of material is high — requires large energy to conduct — called dielectric.

→ In electro magnetics Conductors & dielectrics are defined on basis of ratio of conduction current to displacement current. Ratio of conduction current to displacement current is  $\frac{\sigma}{\omega\epsilon}$ .

\* If  $\frac{\sigma}{\omega\epsilon} = 1$  — b/w conductors & dielectrics.

$\frac{\sigma}{\omega\epsilon} > 1$  — good conductors.

$\frac{\sigma}{\omega\epsilon} < 1$  — dielectrics.



### 2.3. Dielectric Polarization: -

→ dielectric material is divided into two types

(i) polar

(ii) non-polar molecules.

→ molecules whose centre of positive & negative charges coincide - nonpolar

→ molecules whose centre is displaced from each other is polar.

→ when non-polar dielectric material is placed in an electric field - displacement of negative & positive charges takes place in opposite directions & produce a dipole.

→ polarization is defined as dipole moment per unit volume.

$$P = \lim_{\Delta V \rightarrow 0} \frac{1}{\Delta V} \sum_{i=1}^{n\Delta V} P_i \quad \text{C/m}^2$$

→ If the dipoles are aligned in random orientation - polarization has a

2.4. Equipotential Surfaces, EnggTree.com

→ It is an imaginary surface in a electric field of a given <sup>charge</sup> distribution in which all the surface points are having same electric potential.



$$V_1 = V_2 = V_3 = V_4 = V = \frac{Q}{4\pi\epsilon_0 r}$$

$$r_1 = r_2 = r_3 = r_4 = r$$

$$V \propto \frac{1}{r}$$

2.5. Uniform & Non-uniform field :-

$\vec{E}$  at Equipotential Surface } right-angles to each other.

Work done is zero (uniform field).

In a non-uniform field work done will not be zero.



## 2.6 Conduction Current & Displacement Current :-

→ when electric field is applied to a conductor — conduction current occurs due to drift motion of electron. when the electron move they encountered with forces called Resistance.

Current density  $J \rightarrow A/m^2$ .

$$J \propto E, \quad J = \sigma E$$

Since  $J = \frac{I}{s}$   $\downarrow$  conductivity of material

$$\sigma E = \frac{I}{s}, \quad E = \frac{V}{l}, \quad R = \frac{V}{I} = \frac{l}{\sigma s}$$

$$\frac{\sigma V}{l} = \frac{I}{s}, \quad R = \frac{l}{\sigma s}$$

$$\boxed{R = \frac{\rho l}{s}}$$

→ Displacement current  $I_D$  is flowing through a capacitor when ac voltage is applied across the capacitor.

$$I_D = \frac{dQ}{dt}$$

$$= c \frac{dV}{dt}$$

for parallel plate capacitor  $c = \frac{\epsilon_0 A}{d}$



$$\vec{I}_D = \frac{\epsilon_0 A}{d} \cdot \frac{dV}{dt}$$

$$= \epsilon A \frac{dE}{dt} \quad [ \because V = Ed ]$$

$$= A \cdot \frac{\partial D}{\partial t} \quad [ \because D = \epsilon E ]$$

Displacement current density

$$J_D = \frac{\vec{I}_D}{A}$$

$$J_D = \frac{\partial D}{\partial t}$$

2.7. Dielectric Strength :-

→ It is the maximum electric field that a dielectric can tolerate or withstand without electrical breakdown.

2.8. Boundary Conditions :-

→ Conditions existing at the boundary of two medium when field passes from one medium to other.

→ Depending on the nature of medium, it can be classified into three types :-

- (i) Boundary b/w dielectric & dielectric
- (ii) Boundary b/w conductor & dielectric
- (iii) Boundary b/w conductor & free space.

To determine the boundary conditions we need to use Maxwell's equations

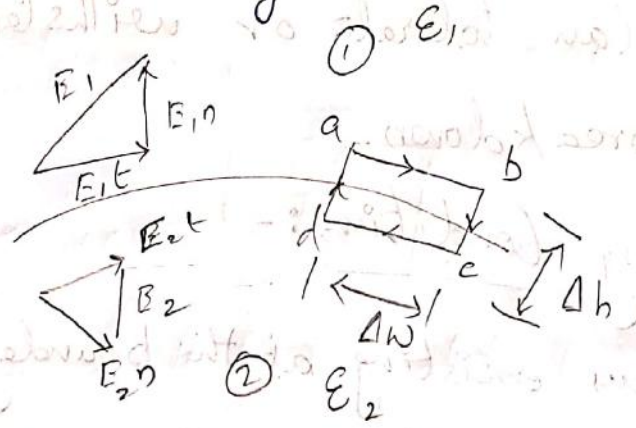
$$\oint E \cdot dl = 0$$

$$\oint_S D \cdot ds = Q_{enc.}$$

free charge enclosed by

the surface.

1) Boundary b/w Dielectric & Dielectric:



Consider a field  $E$  existing in a region that consists of two diff dielectric by

$$E = E_0 \epsilon_r$$

$$E_1 = E_0 \epsilon_{r1}$$

$$E_2 = E_0 \epsilon_{r2}$$



$$E = E_t + E_n, \quad E_1 = E_{1t} + E_{1n}$$

$$E_2 = E_{2t} + E_{2n}$$

→ we apply Maxwell equ to closed loop abcda  $\oint E \cdot dl = 0$

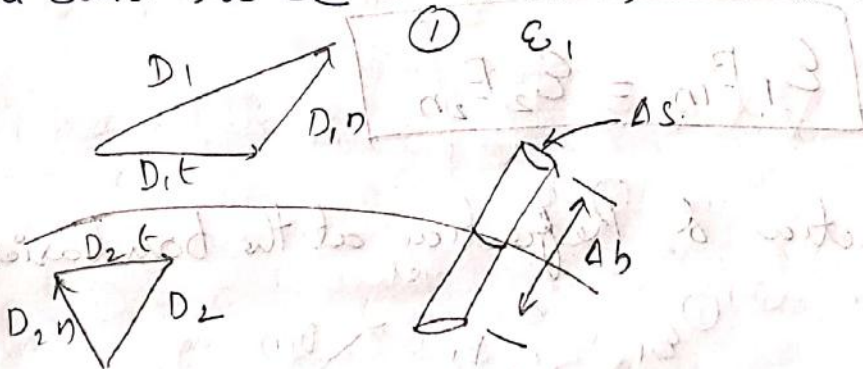
$$0 = E_{1t} \Delta w - E_{1n} \Delta h/2 - E_{2n} \Delta h/2$$

$$+ E_{2t} \Delta w + E_{2n} \Delta h/2$$

$$0 = \Delta w (E_{1t} - E_{2t})$$

$$\Delta h = 0 \Rightarrow E_{1t} = E_{2t}$$

$E_t$  undergoes no change on the boundary & it is said to be continuous across the boundary.



$$D = \epsilon E, \quad \frac{D}{\epsilon} = E$$

$$E_{1t} = \frac{D_{1t}}{\epsilon_1}; \quad E_{2t} = \frac{D_{2t}}{\epsilon_2}$$

$$E_{1t} = E_{2t}, \quad \frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}$$



$D_t$  undergoes some change across the boundary and it is said to be discontinuous across the boundary.

$$\oint_S D \cdot ds = Q_{enc.}$$

Let us assume  $Q_{enc} = 0$

$$\Delta Q = \int_S \Delta S = D_{1n} \Delta S - D_{2n} \Delta S$$

$$\int_S \Delta S = \Delta S (D_{1n} - D_{2n})$$

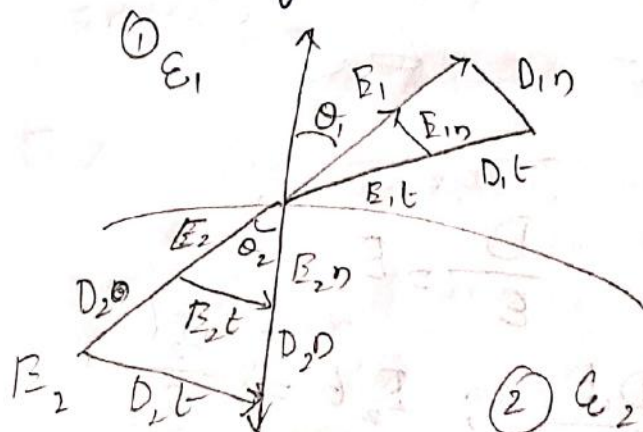
→ If no free charge is enclosed

$$Q_S = 0 \Rightarrow \boxed{D_{1n} = D_{2n}}$$

$D_n$  undergoes no change at the boundary

$$\boxed{E_1 \epsilon_1 = E_2 \epsilon_2}$$

Reflection & Refraction at the boundaries: -



The normal components of  $D$  are given below:

$$D_{n1} = D_1 \cos \theta_1$$

$$D_{n2} = D_2 \cos \theta_2$$

The tangential components of  $E$  are given below,

$$E_{t1} = E_1 \sin \theta_1$$

$$E_{t2} = E_2 \sin \theta_2$$

Apply the boundary condition

$$D_{n1} = D_{n2}$$

$$E_{t1} = E_{t2}$$

$$D_1 \cos \theta_1 = D_2 \cos \theta_2$$

$$E_1 \sin \theta_1 = E_2 \sin \theta_2$$

Dividing  $\frac{E_1 \tan \theta_1}{D_1} = \frac{E_2 \tan \theta_2}{D_2}$

But  $D_1 = \epsilon_1 E_1$  and  $D_2 = \epsilon_2 E_2$

Then  $\frac{E_1 \tan \theta_1}{\epsilon_1 E_1} = \frac{E_2 \tan \theta_2}{\epsilon_2 E_2}$

$$\frac{\tan \theta_1}{\epsilon_1} = \frac{\tan \theta_2}{\epsilon_2}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1}{\epsilon_2}$$



## 2.9. Poisson's AND Laplace's Equations :-

According to Gauss' law point law form, divergence of electric flux density is equal to Volume charge density,

$$\nabla \cdot D = \rho_v$$

$$\text{But } D = \epsilon E$$

$$\nabla \cdot (\epsilon E) = \rho_v$$

$$\epsilon \nabla \cdot E = \rho_v$$

$$\nabla \cdot E = \frac{\rho_v}{\epsilon}$$

$$\text{But } E = -\nabla V$$

$$\nabla \cdot (-\nabla V) = \frac{\rho_v}{\epsilon}$$

$$\boxed{\nabla^2 V = -\frac{\rho_v}{\epsilon}}$$

This is Poisson's Equation.

For Cartesian System

$$\nabla \cdot \nabla V = \frac{\partial}{\partial x} \left( \frac{\partial V}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{\partial V}{\partial y} \right) + \frac{\partial}{\partial z} \left( \frac{\partial V}{\partial z} \right)$$

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} = -\frac{\rho_v}{\epsilon}$$

This is Poisson's equation in Cartesian form



If the volume charge density ( $\rho_v$ ) is zero then

$$\boxed{\nabla^2 V = 0}$$

This is Laplace equation.  $\nabla^2$  operator is called as Laplacian operator.

2.10 Capacitance / Capacitor :-

→ Capacitor is an electrostatic device which consists of two opposite conductor charge density separated by a dielectric medium.

→ Capacitance is the property by which ratio of either charge to potential difference b/w conductor.

$$C = \frac{Q}{V} \rightarrow C/V \Rightarrow \text{Farad.}$$

Assume uniform charge density  $D$  over the plates

$$D = \frac{Q}{A}, \text{ In terms of } E$$

$$D = \epsilon E, \therefore \frac{Q}{A} = \epsilon E, Q = A \epsilon E.$$

But electric field  $E = V/d,$

$$Q = A \epsilon \frac{V}{d}$$

$$\therefore C = \frac{A \epsilon_0 \epsilon_r}{d} \text{ Farad.}$$

2.11. Capacitance of parallel plate capacitor with two electric media.

$$V = V_1 + V_2$$

$$E_1 = \frac{D}{\epsilon_{r1}} = \frac{Q}{A \epsilon_{r1} \epsilon_0}$$

$$E_2 = \frac{D}{\epsilon_{r2}} = \frac{Q}{A \epsilon_{r2} \epsilon_0}$$

The applied potential  $V = E_1 d_1 + E_2 (d - d_1)$

$$V = \frac{Q}{A \epsilon_0} \left[ \frac{d_1}{\epsilon_{r1}} + \frac{d - d_1}{\epsilon_{r2}} \right]$$

$$C = \frac{Q}{V}$$

$$C = \frac{A \epsilon_0 \epsilon_{r1} \epsilon_{r2}}{d_1 \epsilon_{r2} + (d - d_1) \epsilon_{r1}}$$

if medium is air  $\epsilon_{r1} = 1$ ,  $\epsilon_{r2} = \epsilon_r$

$$\therefore C = \frac{A \epsilon_0 \epsilon_r}{d_1 \epsilon_r + (d - d_1)}$$

Three different dielectrics  $\epsilon_{r1}, \epsilon_{r2}, \epsilon_{r3}$ .

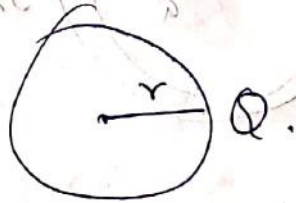
$$C = \frac{A \epsilon_0}{\frac{d_1}{\epsilon_{r1}} + \frac{d_2}{\epsilon_{r2}} + \frac{d_3}{\epsilon_{r3}}}$$



2.11.1

Capacitance of Isolated sphere :-

Consider a sphere of radius 'r'



The potential of sphere is by using

$$V = - \int_{\infty}^r E \cdot dr$$

But  $E = \frac{Q}{4\pi\epsilon_0 r^2}$

$$= - \int_{\infty}^r \frac{Q}{4\pi\epsilon_0 r^2} \cdot dr$$

$$= - \frac{Q}{4\pi\epsilon_0} \int_{\infty}^r \frac{1}{r^2} \cdot dr$$

$$V = \frac{Q}{4\pi\epsilon_0 r}, \quad C = \frac{Q}{V}$$

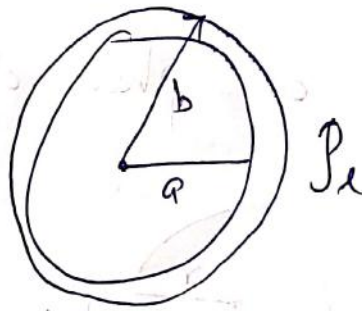
$$C = 4\pi\epsilon_0 r \text{ Farad.}$$

Two concentric spheres of inner radius 'a' & outer radius 'b'

$$C = 4\pi\epsilon_0 \left[ \frac{ab}{b-a} \right]$$



2.11.2. Capacitance of Co-axial Cable :-



Since  $E = \frac{P_1}{2\pi \epsilon_0 r}$

Pd b/w two Co-axial Cable is

$$V = - \int_a^b E dr = \frac{P_1}{2\pi \epsilon_0} \ln\left(\frac{b}{a}\right)$$

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Capacitance of Co-axial Cable is

$$C = P_1 / V$$

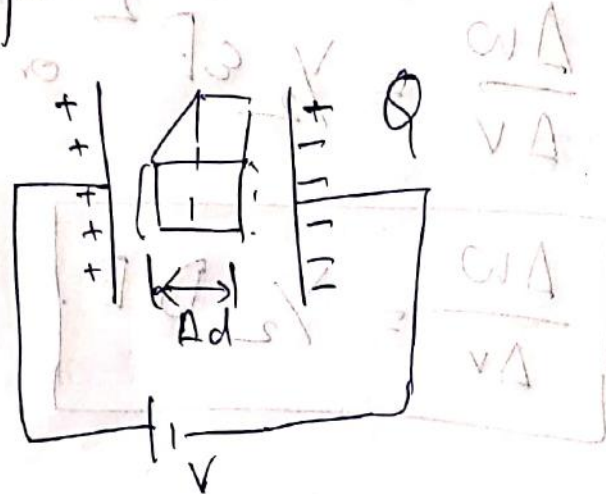
$$C = \frac{2\pi \epsilon_0 \epsilon_r}{\ln(b/a)} \text{ F/m.}$$

2.12. Energy density :-

The stored energy inside a capacitance is in the form of Electrostatic form

$$W = \frac{1}{2} CV^2 = \frac{1}{2} QV \text{ Joules.}$$

EnggTree.com  
 Consider a cube of side  $\Delta d$  parallel to the plates of a capacitor



The capacitance of capacitor is

$$C = \frac{QA}{\Delta V} = \frac{\epsilon(\Delta d)^2 E}{\Delta d}$$

$$C = \epsilon \Delta d$$

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Energy stored  $\Delta W = \frac{1}{2} C (\Delta V)^2$

Pd across the cube is

$$\Delta V = E \cdot \Delta d$$

The stored energy

$$\Delta W = \frac{1}{2} (\epsilon \Delta d) (E \cdot \Delta d)^2$$

$$= \frac{1}{2} \epsilon E^2 (\Delta d)^3$$

$$= \frac{1}{2} \epsilon E^2 \Delta V$$

$$\Delta V = (\Delta d)^3 \text{ is Volume.}$$

Energy density is given by

$$\frac{\Delta W}{\Delta V} = \frac{1}{2} \epsilon E^2 \quad \text{or}$$

$$\boxed{\frac{\Delta W}{\Delta V} = \frac{1}{2} D \cdot E} \quad \text{Joules/m}^3$$

Note: problems refer text book

EMT by Dewan Jayan Page no: 2.54 to  
2.137. (Examples).



3.1

# Magnetic flux & Magnetic flux density (B)

→ Magnetic flux ( $\phi$ ) is defined as magnetic lines of force passing unit Area.

$$\phi = \oint B \cdot ds \text{ weber.}$$

→ Magnetic flux density is defined as density of flux passing per unit Area.

$$B = \phi/A = \text{wb/m}^2 \Rightarrow \text{Tesla.}$$

$$\rightarrow B = \mu H.$$

↳ permeability of medium

$$\mu = \mu_0 \mu_r.$$

↳ permeability of free space

↳ Relative permeability.

$$\mu_0 = 4\pi \times 10^{-7}.$$

H → magnetic field Intensity.

→ Since magnetic flux lines are closed & don't terminate.

→ Gauss law for magnetic field is

$$\oint_S B \cdot ds = 0.$$

By divergence theorem [EnggTree.com](http://EnggTree.com)

$$\iint_S \mathbf{B} \cdot d\mathbf{s} = \nabla \cdot \mathbf{B}$$

Then  $\nabla \cdot \mathbf{B} = 0$

→ total magnetic flux passing through any closed surface is equal to zero.

3.2 Lorentz force :-

→ charged motion particle in a magnetic field experience a force.

→ force is proportional to product of magnitude of charge  $Q$ , its velocity & flux density & sine of angle b/w  $v$  &  $B$ .

$$F = Q(\vec{v} \times \vec{B})$$

$$= BQv \sin \theta.$$

Electric force on a charged particle is

$$F = qE.$$

→ so combine electric & Magnetic field will be

$$F = q\vec{E} + q\vec{v} \times \vec{B}$$

$$F = Q[\vec{E} + \vec{v} \times \vec{B}] \text{ Lorentz force.}$$

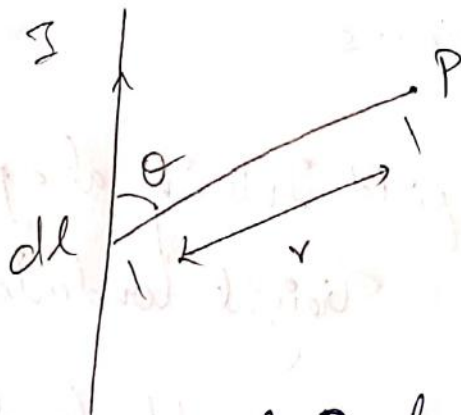
The magnitude of force in

$$F = B I l \sin \theta \quad \text{or}$$

$F = (I \times B) l$ , force on a current element.

3.3. Biot - Savart's Law :-

→ Law states that magnetic flux density produced by a current element at any point in a magnetic field is proportional to the current element & inversely proportional to square of the distance b/w them.



flux density at a point P due to current element  $I dl$  is given by

$$dB \propto \frac{I dl \sin \theta}{r^2}$$

$$dB = \frac{\mu_0}{4\pi} \frac{I dl \sin \theta}{r^2}$$



Magnetic field Intensity is given by

$$dH = \frac{I dl \sin \alpha}{4\pi r^2}$$

3.4. Ampere's Circuital law

Law states that line integral of magnetic field Intensity  $H$  about any closed path is exactly equal to the direct current enclosed by that path.

$$\oint H \cdot dl = I$$

3.5. Applications

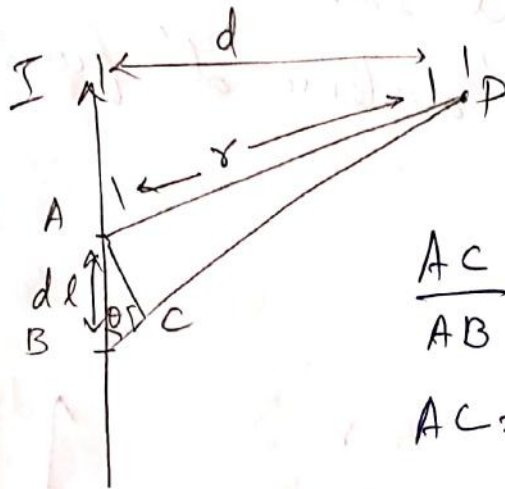
3.5.1. Magnetic field Intensity at a point due to straight conductor.

Consider a long straight conductor carrying current  $I$  and also consider a current element  $I dl$ . Let 'P' be a point at 'B' to measured.

According to Biot-Savart law,

$$B = \frac{\mu_0 I}{4\pi} \int \frac{dl \sin\theta}{r^2}$$

From  $\triangle ABC$



$$\frac{AC}{AB} = \sin\theta$$

$$AC = dl \sin\theta$$

But arc  $AC = r d\theta$ .

$$dl \sin\theta = r d\theta$$

$$d\theta = \frac{dl \sin\theta}{r}$$

Sub this value in 'B' equation.

$$B = \frac{\mu_0 I}{4\pi} \int \frac{d\theta}{r} \quad [\text{from figure } d/r = \sin\theta]$$

$$\text{So } B = \frac{\mu_0 I}{4\pi d} \int_0^\pi \sin\theta d\theta$$

$$= \frac{\mu_0 I}{4\pi d} [-\cos\theta]_0^\pi$$

$$B = \frac{\mu_0 I}{4\pi d} \times 2 = \frac{\mu_0 I}{2\pi d} \quad \underline{\underline{\text{wb/m}^2}}$$

3.5.2 Magnetic flux density at any point along the axis of circular coil/loop:-

→ Consider a circular coil of radius 'a' carrying a current  $I$  and also consider current element  $I dl$ , let 'P' be any point on 'B' distance 'd' from the centre of coil



→ Magnetic flux density 'B' at point 'P' due to current element  $dl$  is

$$dB = \frac{\mu_0 I dl}{4\pi r^2}$$

$$\text{From } \triangle AOP \quad r^2 = a^2 + d^2$$

$$\begin{aligned} dB &= dB \cos \theta \\ &= dB \cdot \frac{a}{\sqrt{a^2 + d^2}} \\ &= \frac{\mu_0 I dl}{4\pi r^2} \times \frac{a}{\sqrt{a^2 + d^2}} \end{aligned}$$



$$dB = \frac{\mu_0 I a}{4\pi (a^2 + d^2)^{3/2}} \times \frac{dl}{\sqrt{a^2 + d^2}}$$

$$dB = \frac{\mu_0 a I dl}{4\pi (a^2 + d^2)^{3/2}}$$

Magnetic flux density due to Circular Coil is given by

$$B = \frac{\mu_0 a I}{4\pi (a^2 + d^2)^{3/2}} \int dl$$

$$= \frac{\mu_0 a I}{4\pi (a^2 + d^2)^{3/2}} \times 2\pi a$$

$$B = \frac{\mu_0 a^2 I}{2(a^2 + d^2)^{3/2}} \text{ Wb/m}^2$$

$$H = \frac{I a^2}{2(a^2 + d^2)^{3/2}} \text{ A/m}$$

If  $d = 0$ , field at centre

$$B = \frac{\mu_0 a^2 I}{2a^3} = \frac{\mu_0 I}{2a}$$

$$H = \frac{I}{2a} \text{ A/m}$$

3.6

## Magnetic potential

(i) Scalar magnetic potential :-

$$\rightarrow \oint H \cdot dl = I$$

If no current is enclosed in  $I = 0$

$$\oint H \cdot dl = 0$$

Magnetic field  $H$  can be expressed as negative gradient of a scalar function

$$H = -\nabla V_m$$

$V_m \rightarrow$  Scalar magnetic potential

$$V_m = -\int H \cdot dl$$

This also satisfies Laplace equation.

$$\text{In free space } \nabla \cdot B = 0$$

$$\mu_0 \nabla \cdot H = 0$$

$$\text{But } H = -\nabla V_m$$

$$\mu_0 \nabla \cdot (-\nabla V_m) = 0$$

$$-\mu_0 \nabla^2 V_m = 0$$

$$\nabla^2 V_m = 0$$

(ii) Vector magnetic potential

→ If current is enclosed, the potential depends upon current element.

→ Since divergence of a vector is a scalar, vector potential is expressed in curl

$$\text{i.e., } \nabla \cdot \mathbf{B} = 0$$

$$\mathbf{B} = \nabla \times \mathbf{A} \quad \text{--- (1)}$$

$\mathbf{A}$  → magnetic vector potential.

Take curl on both sides in eq (1)

$$\nabla \times \mathbf{B} = \nabla \times \nabla \times \mathbf{A}$$

By the identity  $\nabla \times \nabla \times \mathbf{A} = \nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}$ .

But  $\nabla \times \mathbf{B} = \mu \mathbf{J}$

$$\nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A} = \mu \mathbf{J}$$

for the steady dc  $(\nabla \cdot \mathbf{A}) = 0$

then  $-\nabla^2 \mathbf{A} = \mu \mathbf{J}$

Equating

$$\begin{aligned} \nabla^2 A_x &= -\mu J_x \\ \nabla^2 A_y &= -\mu J_y \\ \nabla^2 A_z &= -\mu J_z \end{aligned}$$



→ In form of Poisson's equation.

Magnetic Vector potential can be written as

$$A_x = \frac{\mu}{4\pi} \int_V \left( \frac{J_x}{r} \right) dv$$

$$A_y = \frac{\mu}{4\pi} \int_V \left( \frac{J_y}{r} \right) dv$$

$$A_z = \frac{\mu}{4\pi} \int_V \left( \frac{J_z}{r} \right) dv.$$

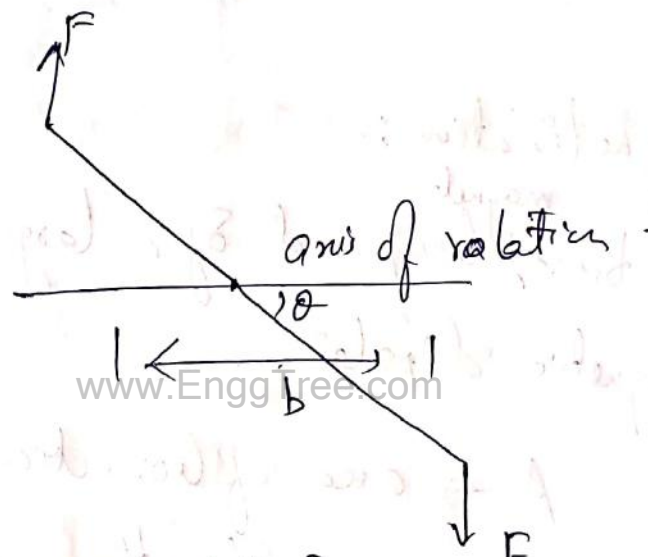
In general vector potential can be expressed as

$$A = \frac{\mu}{4\pi} \iiint \frac{\mathbf{J}}{r} dv.$$

### 3.7 Magnetic Torque

→ when a current loop placed in a magnetic field, forces act on the loop — tend to rotate it.

→ Consider a rectangular loop of length 'l' & breadth 'b' carrying a current 'I' in a uniform magnetic field 'B'.



force  $F = B I l \sin \theta$

→ loop plane is parallel to the magnetic field

Total torque  $T = 2 \times \text{torque on each side}$

$$= 2 \times \text{force} \times \text{distance}$$

$$= 2 B I l \sin \theta \cdot b/2$$

$$= B I l b \sin \theta$$

$$T = B I A \sin \theta \quad (A = lb)$$

Magnetic moment  $\vec{m} = I A \hat{n}$

$$m = I A ; T = m B \sin \theta \hat{n}$$

$$T = \vec{m} \times \vec{B}$$

## 3.8 Magnetic dipole :-

→ pole strength  $Q_m$  & length  $l$   
 In a small bar magnet is treated as  
 magnetic dipole

Since  $\therefore m = IA$

$$\boxed{\therefore Q_m l = IA}$$

## 3.9. Magnetization :-

→ bar<sup>magnet</sup> composed of a large number of a  
 magnetic dipoles

$A$  → area of cross section

$l$  → axial length

$Al$  → Volume.

$Q_m l$  → dipole moment.

→ net dipole moment per unit volume.

∴ Magnetization. ( $M$ )

$$M = \frac{Q_m l}{\text{Volume}} = \frac{Q_m}{A}$$

Magnetic susceptibility

$$\chi_m = M/H$$



In free space flux density is given by

$$B = \mu_0 H.$$

for magnet, flux density is given by.

$$B = \mu_0 (H + m)$$

$$= \mu_0 H (1 + m/H)$$

$$= \mu_0 H (1 + \chi_m) \quad \text{--- (1)}$$

Since  $B = \mu_0 H$ , eq (1) becomes.

$$\mu_0 = \mu_0 (1 + \chi_m)$$

$$\boxed{\mu_r = 1 + \chi_m}$$

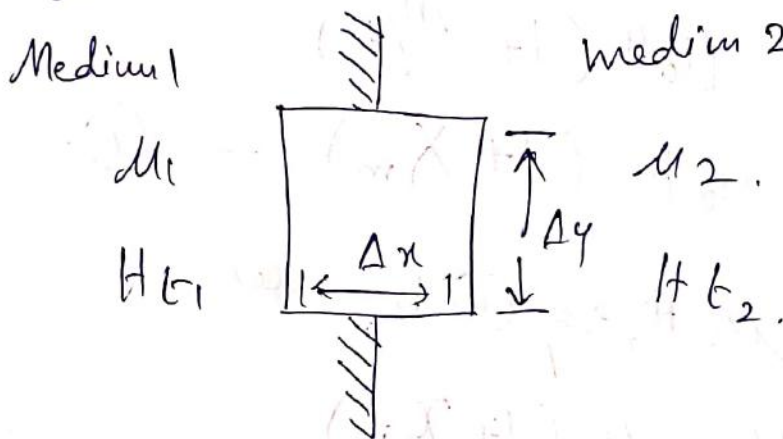
3.10. Magnetic Materials :-

→ Depending on the magnetic behaviour, substances are classified into

- (i) diamagnetic ( $\mu_r \leq 1$ )
- (ii) paramagnetic ( $\mu_r \geq 1$ )
- (iii) ferromagnetic ( $\mu_r \gg 1$ )

(1) Tangential component of magnetic field Intensity is continuous

2) Normal component of  $B$  is continuous across the boundary.



According to Ampere's law,

$$\oint H \cdot dl = I$$

If there is no current enclosed by the path

$$\oint H \cdot dl = 0$$

$$H_{t1} \Delta y - H_{t2} \Delta y = 0$$

$$H_{t1} = H_{t2}$$

Let  $B_{n1}$  — normal component in 1  
 $B_{n2}$  — " " in 2.

By Gauss law for magnetic field.

$$\iint_S \mathbf{B} \cdot d\mathbf{s} = 0$$

$$B_{n1} ds - B_{n2} ds = 0$$

$$B_{n1} = B_{n2}$$

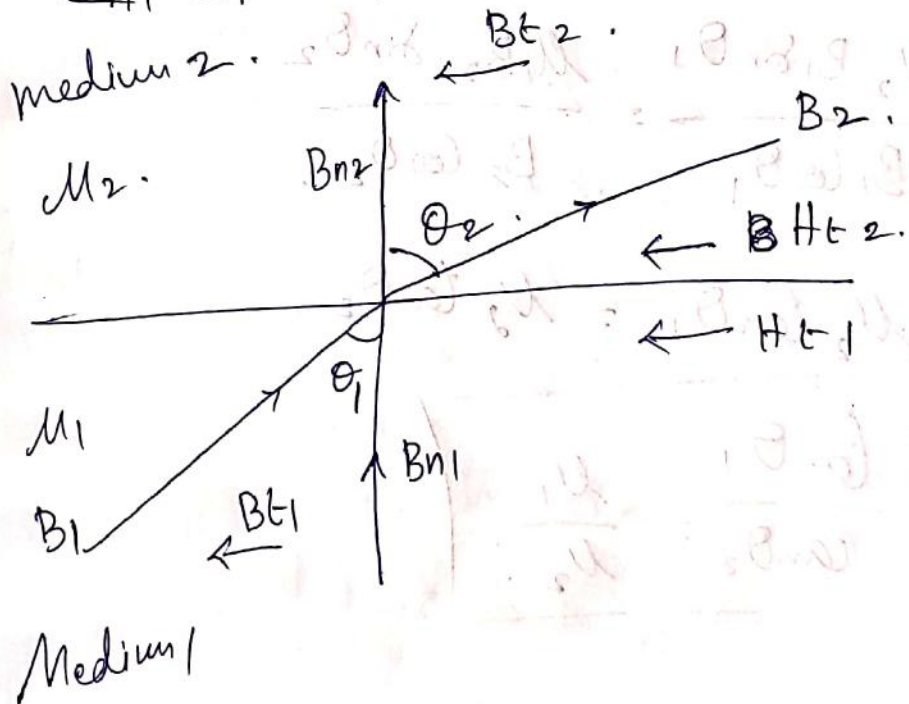
$$B_{n1} = B_1 \cos \theta_1$$

$$B_{n2} = B_2 \cos \theta_2$$

But  $B_{n1} = B_{n2}$

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$$B_1 \cos \theta_1 = B_2 \cos \theta_2 \quad \text{--- (1)}$$





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$$H_{t1} = B_{t1} / \mu_1$$

$$H_{t2} = B_{t2} / \mu_2$$

But  $H_{t1} = H_{t2}$  (Boundary Condition)

$$\frac{B_{t1}}{\mu_1} = \frac{B_{t2}}{\mu_2}$$

$$\mu_2 B_{t1} = \mu_1 B_{t2}$$

When we substitute

$$\mu_2 B_1 \sin \theta_1 = \mu_1 B_2 \sin \theta_2 \quad \text{--- (2)}$$

Divide (2) by (1)

$$\frac{\mu_2 B_1 \sin \theta_1}{B_1 \cos \theta_1} = \frac{\mu_1 B_2 \sin \theta_2}{B_2 \cos \theta_2}$$

$$\mu_2 \tan \theta_1 = \mu_1 \tan \theta_2$$

$$\boxed{\frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_1}{\mu_2}}$$

3.12. Inductance :- EnggTree.com

→ ratio of total flux linkage to the current producing the flux is called inductance.

$$L = \frac{N\phi}{I}$$

→ Inductance of solenoid

$$\text{Total flux linkage} = N\phi$$

$$\phi = BA$$

$$= NBA$$

$$B = \mu H$$

$$\therefore \text{Total flux linkage} = N\mu HA$$

field intensity is given by for solenoid

$$= N\mu \frac{NI}{l} A$$

$$= \frac{\mu N^2 I A}{l}$$

$$H = \frac{NI}{l}$$

$$\text{Inductance} = \frac{\mu N^2 I A}{l I}$$

$$L = \frac{\mu N^2 A}{l}$$

→ Inductance of cord:-

$$\text{Total flux linkage} = N\phi$$

$$\phi = BA.$$

$$= NB A$$

$$= N\mu H A.$$

$$H = \frac{NI}{2\pi R} = \frac{N\mu NI A}{2\pi R}$$

$$H = \frac{\mu N^2 I A}{2\pi R}$$

$$L = \frac{\mu N^2 I A}{2\pi R I}$$

$$L = \frac{\mu N^2 A}{2\pi R}$$

$$\boxed{L = \frac{N^2 R}{2}}$$

For co-axial cable

$$\boxed{L = \frac{\mu d \ln(b/a)}{2\pi}} \quad H.$$



Reluctance

$$R = \frac{\text{mmf}}{\text{Total flux}} = \frac{e_m}{\phi}$$

$$R = \frac{l}{\mu_s}$$

$$\text{Permeance } P = \frac{1}{R} = \frac{\phi}{e_m} = \frac{\mu_s}{l}$$

$$\text{mmf} = \phi \times R$$

$$\text{mmf} = H \times l$$

3.13.

Magnetic Energy:-

$$W = \frac{1}{2} LI^2$$

$$W_m = \frac{1}{2} \Delta L (AI)^2$$

$$dw = v i dt$$

Energy stored in magnetic field

$$W = \int_0^I v i dt$$

$$= \int_0^I L \frac{di}{dt} i dt$$

$$W = \frac{1}{2} LI^2$$

Energy Density

EnggTree.com

Note: problems

page - 3.27 to 3.48  
&  
page - 4.25 to 4.46

$$W = \frac{1}{2} LI^2$$

Inductance of the Solenoid is given by

$$L = \frac{\mu_0 N^2 A}{l}$$

Sub in above equation

$$W = \frac{1}{2} \frac{\mu_0 N^2 A}{l} I^2$$

$$= \frac{1}{2} \mu_0 \left( \frac{NI}{l} \right)^2 l A$$

$$W = \frac{1}{2} \mu_0 H^2 l A \quad \left[ \because H = \frac{NI}{l} \right]$$

Energy stored per unit volume

$$w = \frac{1}{2} \mu_0 H^2$$

$$= \frac{1}{2} (\mu_0 H) \cdot H$$

$$w = \frac{1}{2} B \cdot H$$

The energy stored

$$W = \int w dv$$

$$W = \int \frac{1}{2} \mu H^2 dv$$

4.1

→ Magnetic flux are continuous & forms closed paths — a single line flux called magnetic circuit.

→ Magnetic flux through magnetic circuit is defined as ratio of magnetomotive force to Reluctance of the magnetic circuit.

$$\text{Magnetic flux} = \frac{\text{MMF}}{\text{Reluctance}} \quad (\text{Magnetic Ohm's law})$$

→ Reluctance is the opposition to the flux path in a magnetic circuit

→ It is also the Ratio of total MMF to the flux through it.

$$\text{Reluctance} = \frac{\text{MMF}}{\text{magnetic flux}}$$

$$S = \frac{\oint H \cdot dl}{BA}$$

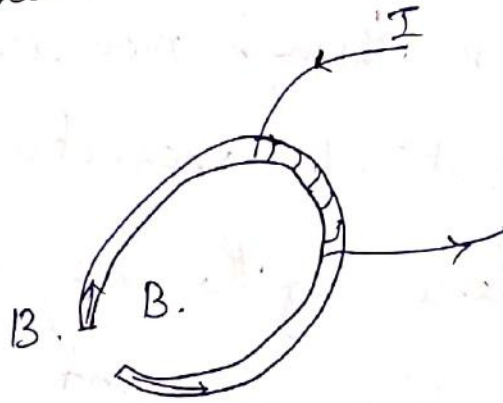
$$S = \frac{Hl}{BA} = \frac{Hl}{\mu HA} = \frac{l}{\mu A} \text{ H}^{-1}$$



Reciprocal of Permeance

$$P = \frac{1}{\mathcal{P}} = \frac{\mu A}{l} \text{ Henry.}$$

Magnetic circuit with air gap :-



→ thickness 't'

→ B - flux density in the gap is same as in the iron.

→ field Intensity in the iron is

$$H_i = \frac{B}{\mu} = \frac{B}{\mu_0 \mu_r}$$

and the field Intensity in the air gap is

$$H_g = \frac{B}{\mu_0}$$

Note :- problems in Dhawanjayan (Text)

Page - 4.25 to 4.43.

4.2

FARADAY'S LAW AND ITS IMPLEMENTATION

Total electromotive force (emf) induced in a circuit is equal to the rate of decrease of total magnetic flux linking the circuit.

$$V = - \frac{d\phi}{dt}$$

→ N number of turns, then total flux is  $N\phi$ , where  $\phi$  is the magnetic flux

$$V = -N \frac{d\phi}{dt}$$

→ with reference to definition, the emf in a circuit is the line integral of the electric field around the closed path

$$V = \oint E \cdot dl$$

↳ Electric field.

→ According to Gauss law

$$\phi = \iint B \cdot ds$$

Sub the value of  $\phi$  in emf equation

$$V = -\frac{d}{dt} \iint B \cdot ds$$

$$V = -\iint \frac{\partial B}{\partial t} \cdot ds$$

But  $V = \oint E \cdot dl$

$$\oint E \cdot dl = -\iint_S \frac{\partial B}{\partial t} \cdot ds$$

Applying Stokes theorem

$$\oint E \cdot dl = \iint_S \nabla \times E \cdot ds$$

Then

$$\iint_S \nabla \times E \cdot ds = -\iint_S \frac{\partial B}{\partial t} \cdot ds$$

$$\nabla \times E = -\frac{\partial B}{\partial t}$$

This is referred to Maxwell equation.



## 4.2.1. Self Inductance & Mutual Inductance:-

→ changing current will produce an induced emf in the circuit to oppose the change in flux — this phenomenon is Self Inductance.

Consider a coil having 'N' number of turns — if AC is applied

Induced emf is proportional to rate of change of current

$$V \propto \frac{di}{dt}$$

$$V = L \frac{di}{dt}$$

$$L \frac{di}{dt} = N \frac{d\phi}{dt} \quad (\text{since } \phi \Rightarrow V = \frac{N d\phi}{dt})$$

$$L = N \frac{d\phi}{di}$$

$$\therefore \boxed{L = \frac{N\phi}{i}}$$

Mutual Inductance is the ratio of induced magnetic flux linkage in one coil to the current through other coil.

$$M = N_1 \frac{\phi_{21}}{i_2}$$

&

$$M = N_2 \frac{\phi_{21}}{i_1}$$

Co-efficient of coupling

$$k = \frac{M}{\sqrt{L_1 L_2}} \quad (k \text{ is always less than } 1)$$

### 4.3 Maxwell's Equations

→ Maxwell derived the concept of magnetic field produced by changing Electric field.

→ four electromagnetic Equations called Maxwell's Equations

→ It has both Integral & differential form

→ these equations are based on fundamental laws of Gauss, Faraday & Ampere.

→ Each differential equation has its Integral Counter part.

From Ampere's Circuital law:-

→ line Integral of the magnetic field Intensity  $H$  on any closed path is equal to current enclosed by that path.

$$\oint H \cdot dl = I$$

$$= \iiint_S J \cdot ds.$$

Total current involves both conduction current and displacement current.

→ current through resistive element is called conduction current.

→ current through capacitive element is called displacement current.

Conduction current density

$$I_c = \frac{V}{R}$$

$$\text{But } R = \frac{\rho l}{A} = \frac{l}{\sigma A}$$

↳ conductivity.



$$\therefore \frac{V\sigma A}{l} = I_c$$

If  $E$  is the electric field, then

Voltage  $V = E \cdot l$

$$I_c = \frac{E l \sigma A}{l}$$

$$I_c = E \sigma A$$

$$\frac{I_c}{A} = E \sigma, \quad \boxed{J_c = \sigma E} \quad \text{--- (1)}$$

Displacement current density

$$I_D = \frac{dQ}{dt}$$

$$Q = CV \Rightarrow I_D = C \frac{dV}{dt}$$

Since  $C = \frac{\epsilon_0 A}{d}$

Sub in above equation

$$I_D = \frac{\epsilon_0 A}{d} \cdot \frac{dV}{dt}$$

But  $V = Ed$

$$I_D = \frac{\epsilon_0 A}{d} \cdot d \frac{dE}{dt}$$

$$I_D = \epsilon A \frac{dE}{dt}$$

$$\frac{I_D}{A} = \epsilon \frac{\partial E}{\partial t}$$

$$= \frac{\partial D}{\partial t} \quad [\because D = \epsilon E]$$

Displacement current density

$$J_D = I/A \text{ is}$$

$$\boxed{J_D = \frac{\partial D}{\partial t}} \quad - (2)$$

Equation (1) & (2) are the Differential forms.

Ampere law can be written as

$$\oint H \cdot dl = \iint_S (J_c + J_D) ds.$$

$$\text{then } \oint H \cdot dl = \iint_S (\sigma E + \frac{\partial D}{\partial t}) ds.$$

$$\oint H \cdot dl = \iint_S [\sigma E + \epsilon \frac{\partial E}{\partial t}] ds.$$

$$\text{then } \oint H \cdot dl = \iint_S (J + \frac{\partial D}{\partial t}) ds.$$

This is the Maxwell's equation in integral form from Ampere law.

By Applying <sup>EnggTree.com</sup> Stokes Theorem

$$\oint H \cdot dl = \iint_S \nabla \times H \cdot ds$$

Comparing above two equations

$$\iint_S \nabla \times H \cdot ds = \iint_S \left[ J + \frac{\partial D}{\partial t} \right] \cdot ds$$

$$\nabla \times H = J + \frac{\partial D}{\partial t}$$

$$\nabla \times H = \sigma E + \epsilon \frac{\partial E}{\partial t}$$

Maxwell's equation in differential form.

Statement :- mmf around a closed path is equal to the sum of the conduction current & displacement current enclosed by the path.



From Faraday's law :-

As Faraday's law states,

$$V = - \frac{d\phi}{dt}$$

$$= \frac{d}{dt} \left( \iint_S B \cdot ds \right)$$

But

$$V = \oint E \cdot dl$$

$$\oint E \cdot dl = - \frac{d}{dt} \iint_S B \cdot ds$$

$$\oint E \cdot dl = - \iint_S \frac{\partial B}{\partial t} \cdot ds$$

$$\text{or } \oint E \cdot dl = - \mu \iint_S \frac{\partial H}{\partial t} \cdot ds \text{ (Integral form)}$$

By Applying Stokes theorem

$$\oint E \cdot dl = \iint_S \nabla \times E \cdot ds$$

Comparing both equations

$$\iint_S \nabla \times E \cdot ds = - \iint_S \frac{\partial B}{\partial t} \cdot ds$$

$$\nabla \times E = -\frac{\partial B}{\partial t}$$

$$\nabla \times E = -\mu \frac{\partial H}{\partial t} \quad (\text{differential form}).$$

Statement :- Emf around a closed path is equal to magnetic displacement (flux density) through that closed path.

### 4.3.3. Maxwell's Equation - III

From electric Gauss law,

$$K = Q.$$

$$\iint_S D \cdot ds = Q.$$

$$\text{Or } \iiint_V P_v \cdot dv = Q.$$

Then

$$\iint_S D \cdot ds = \iiint_V P_v \cdot dv \quad (\text{Integral form}).$$

By Applying Divergence theorem

$$\iint_S D \cdot ds = \iiint_V \nabla \cdot D \cdot dv$$

Comparing both equations. EnggTree.com

$$\iiint_V \nabla \cdot D \, dv = \iiint_V \rho \, dv.$$

$$\boxed{\nabla \cdot D = \rho} \text{ differential form.}$$

statement :- Total electric displacement through the surface enclosing a volume is equal to the total charge within the volume.

4.3.4 Maxwell's Equation - IV

From magnetic Gauss law,

$$\phi = 0. \text{ (or)}$$

$$\iint_S B \cdot ds = 0. \text{ (Integral form)}$$

Applying Divergence theorem

$$\iint_S B \cdot ds = \iiint_V \nabla \cdot B \, dv$$

Comparing both equations



$$\iiint_V \nabla \cdot B = 0.$$

$$\boxed{\nabla \cdot B = 0} \quad \text{differential form.}$$

Statement :- net magnetic flux emerging through any closed surface is zero.

4.3.5. Time Varying field :-

→ Electric & Magnetic fields are assumed to be time varying fields.

→ So it is expressed in phasor quantity.

$$E(x, t) = \text{Real part of } [E(x) e^{j\omega t}]$$

$$\frac{\partial E}{\partial t}(x, t) = \text{Real part of } (j\omega E(x) e^{j\omega t})$$

Apply in Maxwell equation

$$\text{Real part of } [\nabla \times H] = \text{Real part of}$$

$$[(\sigma E + j\omega \epsilon E) e^{j\omega t}]$$

$$\nabla \times H = \sigma E + j\omega \epsilon E$$

$$\boxed{\nabla \times H = (\sigma + j\omega \epsilon)E} \quad \text{--- (1)}$$

For magnetic field

$$H(x, t) = \text{Re} [ H(x) e^{j\omega t} ]$$

$$\frac{\partial H}{\partial t}(x, t) = \text{Re} [ j\omega H(x) e^{j\omega t} ]$$

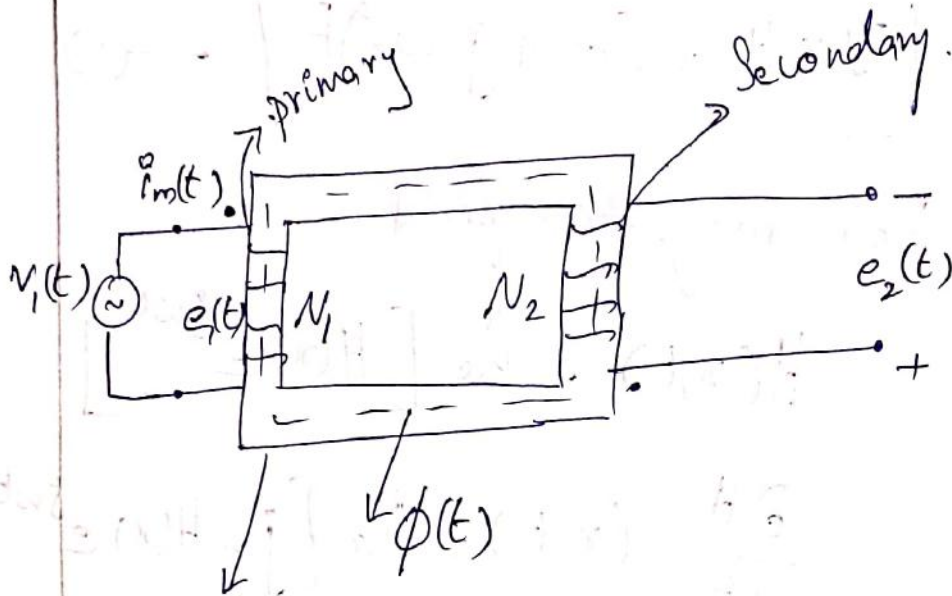
Apply in Maxwell equations

$$\text{Re} [\nabla \times E] = [ -\text{Re} (j\omega \mu H e^{j\omega t}) ]$$

$$\boxed{\nabla \times E = -j\omega \mu H} \quad \text{--- (2)}$$

∴ Note: Maxwell's equations will change incorporating the eq (1) & (2).

# 4.4. Transformer and Mutual Emf.



→ If  $N_1$  &  $N_2$  are the number of turns in primary & Secondary windings respectively, the induced emf's are.

$$e_1 = N_1 \frac{d\phi}{dt}$$

$$e_2 = N_2 \frac{d\phi}{dt}$$

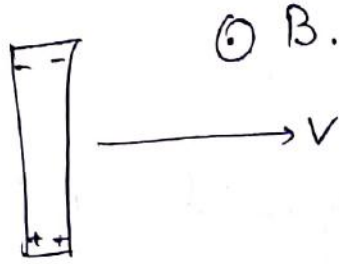
$$\frac{e_1}{e_2} = \frac{N_1}{N_2} \quad (\text{emf ratio})$$

$$\frac{V_1}{V_2} = \frac{N_1}{N_2} = a \quad (\text{Voltage ratio})$$

$$(\text{Current ratio}) \quad \frac{i_2}{i_1} = \frac{V_1}{V_2} = \frac{e_1}{e_2} = \frac{N_1}{N_2}$$



→ Motional emf :-



Consider a conductor moving in a steady magnetic field.

→ if a charge  $Q$  moves in a magnetic field  $\vec{B}$  experiences a force.

$$\vec{F} = Q(\vec{v} \times \vec{B})$$

This force will cause the electrons in conductor to drift towards one end & leave other end positively charged. When  $E$  &  $B$  forces reaches equilibrium, net force on the moving conductor is zero.

$$\frac{\vec{F}}{Q} = \vec{v} \times \vec{B} \quad \text{--- called}$$

motional emf.  $\vec{E}_m = \vec{v} \times \vec{B}$ .

The generated emf around the circuit is  $\oint_c \vec{v} \times \vec{B} \cdot d\vec{l}$  → motional emf.

# 4.5. Relation between field theory & Circuit theory.

Circuit theory	field theory
1. Analysis originated by its own.	1. Evolved from Transmission Theory.
2. Applicable for portion of RF range.	Beyond RF range.
3. dependent & independent parameter, I & V are directly obtained.	3. Not directly obtained, through E & H.
4. parameter of medium are not involved.	parameter are involved [E & H].
5. Laplace transform is employed.	5. Maxwell equations is employed.
6. Z, Y, H parameter are used.	S parameter is used.
7. Low power calculation.	Relatively high power.
8. Simple to understand.	need Visualization ability.
9. Two dimensional.	Three dimensional Analysis.
10. Freq for reference.	wave length for reference.
11. lumped components used.	Distributed components used.

## 5.1 Electromagnetic wave Equation:

→ application of Maxwell's equations -  
existence of electromagnetic wave.

→ wave equation can be derived from  
Maxwell's equation from Faraday's law  
in point form,

$$\begin{aligned}\nabla \times \mathbf{E} &= -\frac{\partial \mathbf{B}}{\partial t} \\ &= -\mu \frac{\partial \mathbf{H}}{\partial t}.\end{aligned}$$

Take curl on both sides,

$$\nabla \times \nabla \times \mathbf{E} = \mu \nabla \times \frac{\partial \mathbf{H}}{\partial t} \quad \text{--- (1)}$$

But Maxwell's equation from Ampere's  
law is

$$\begin{aligned}\nabla \times \mathbf{H} &= \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \\ &= \sigma \mathbf{E} + \epsilon \frac{\partial \mathbf{E}}{\partial t}.\end{aligned}$$

Differentiate

$$\begin{aligned}\nabla \times \frac{\partial \mathbf{H}}{\partial t} &= \frac{\partial \nabla \times \mathbf{H}}{\partial t} \\ &= \frac{\partial}{\partial t} \left( \sigma \mathbf{E} + \epsilon \frac{\partial \mathbf{E}}{\partial t} \right)\end{aligned}$$



$$\nabla \times \frac{\partial H}{\partial t} = \sigma \frac{\partial E}{\partial t} + \epsilon \frac{\partial^2 E}{\partial t^2} \quad \text{--- (2)}$$

Sub (2) in (1) we get.

$$\begin{aligned} \nabla \times \nabla \times E &= -\mu \left[ \sigma \frac{\partial E}{\partial t} + \epsilon \frac{\partial^2 E}{\partial t^2} \right] \\ &= -\mu \sigma \frac{\partial E}{\partial t} - \mu \epsilon \frac{\partial^2 E}{\partial t^2} \quad \text{--- (3)} \end{aligned}$$

But according to the identity

$$\nabla \times \nabla \times E = \nabla (\nabla \cdot E) - \nabla^2 E \quad \text{--- (4)}$$

But

$$\nabla \cdot E = \frac{1}{\epsilon} \nabla \cdot D$$

Since no net charge within the conductor,  $\rho = 0$

$$\nabla \cdot D = 0$$

$$\nabla \cdot E = 0$$

Then equation (4) becomes

$$\nabla \times \nabla \times E = -\nabla^2 E \quad \text{--- (5)}$$

Comparing the equations (3) & (5)

$$\nabla^2 E = \mu\sigma \frac{\partial E}{\partial t} + \mu\epsilon \frac{\partial^2 E}{\partial t^2}$$

$$\nabla^2 E - \mu\sigma \frac{\partial E}{\partial t} - \mu\epsilon \frac{\partial^2 E}{\partial t^2} = 0 \quad \text{--- (6)}$$

This is the wave equation for electric field 'E'.

Wave equation for magnetic field 'H' can be obtained in a similar manner as

$$\nabla^2 H - \mu\sigma \frac{\partial H}{\partial t} - \mu\epsilon \frac{\partial^2 H}{\partial t^2} = 0. \quad \text{--- (7)}$$

Equations (6) & (7) are the wave equations from Maxwell equations.

5.2. Wave equation for free space :-

→ for free space ( $\sigma = 0$ ) &  $\rho = 0$

→ electromagnetic wave equations for free space can be obtained from Maxwell equations.

Maxwell equation from Faraday's Law

$$\begin{aligned}\nabla \times E &= -\frac{\partial B}{\partial t} \\ &= -\mu \frac{\partial H}{\partial t}\end{aligned}$$

Taking curl on both sides

$$\nabla \times \nabla \times E = -\mu \nabla \times \frac{\partial H}{\partial t} \quad \text{---(8)}$$

But Maxwell's equation from Ampere's law for free space is

$$\begin{aligned}\nabla \times H &= \frac{\partial D}{\partial t} \\ &= \epsilon \frac{\partial E}{\partial t}\end{aligned}$$

Then

$$\begin{aligned}\nabla \times \frac{\partial H}{\partial t} &= \frac{\partial \nabla \times H}{\partial t} \\ &= \frac{\partial}{\partial t} \left( \epsilon \frac{\partial E}{\partial t} \right) \\ \nabla \times \frac{\partial H}{\partial t} &= \epsilon \frac{\partial^2 E}{\partial t^2} \quad \text{---(9)}\end{aligned}$$



$$\nabla \times \nabla \times E = -\mu \epsilon \frac{\partial^2 E}{\partial t^2} \quad \text{--- (10)}$$

But by the identity

$$\nabla \cdot E = \frac{1}{\epsilon} \nabla \cdot D = \frac{\rho}{\epsilon} = 0$$

Then  $\nabla \times \nabla \times E = -\nabla^2 E \quad \text{--- (11)}$

Comparing equations (10) & (11)

$$\nabla^2 E = \mu \epsilon \frac{\partial^2 E}{\partial t^2}$$

$$\nabla^2 E - \mu \epsilon \frac{\partial^2 E}{\partial t^2} = 0. \quad \text{--- (12)}$$

Similarly

$$\nabla^2 H - \mu \epsilon \frac{\partial^2 H}{\partial t^2} = 0 \quad \text{--- (13)}$$

Equations (12) & (13) wave equations for free space in terms of electric & magnetic field.

For free space  $\mu_r = 1$  &  $\epsilon_r = 1$  (air)

Wave equation becomes

$$\nabla^2 H - \mu_0 \epsilon_0 \frac{\partial^2 H}{\partial t^2} = 0.$$

$$\mu_0 \epsilon_0 = 4\pi \times 10^{-7} \times \frac{1}{36\pi \times 10^9}$$

$$= \frac{1}{9 \times 10^{16}}$$

$$\frac{1}{\sqrt{\mu_0 \epsilon_0}} = 3 \times 10^8 \text{ m/sec.}$$

$$= v \text{ — velocity of light.}$$

Then wave equation becomes

$$\nabla^2 H - \frac{1}{v^2} \frac{\partial^2 H}{\partial t^2} = 0 \text{ or}$$

$$\nabla^2 E - \frac{1}{v^2} \frac{\partial^2 E}{\partial t^2} = 0.$$

5.3. characteristic impedance or Intrinsic Impedance ( $\eta_0$ )

Consider the wave propagating in x-direction

So,

$$\frac{\partial^2 E}{\partial x^2} = \mu_0 \epsilon_0 \frac{\partial^2 E}{\partial t^2}$$

The solution of this differential equation is

$$E = f_1(x - v_0 t) + f_2(x + v_0 t)$$

$$\text{where } v_0 = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

Solution (consider of two waves,

consider wave in positive direction

$$f_2(x + v_0 t) = 0 \quad (\text{negative direction})$$

The general solution becomes

$$E = f(x - v_0 t)$$

$$\nabla \times E = \begin{vmatrix} \vec{x} & \vec{y} & \vec{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_x & E_y & E_z \end{vmatrix}$$

$$= \vec{x} \left[ \frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} \right] + \vec{y} \left[ \frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} \right] \\ + \vec{z} \left[ \frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right]$$

Since wave travelling in x-direction

y & z are independent

$$E_x = H_x = 0 \quad \text{and} \quad \frac{\partial E}{\partial y} = \frac{\partial E}{\partial z} = 0$$

$$\nabla \times E = - \frac{\partial E_z}{\partial x} \vec{y} + \frac{\partial E_y}{\partial x} \vec{z}$$



$$\nabla \times H = - \frac{\partial H_z}{\partial x} \vec{y} + \frac{\partial H_y}{\partial x} \vec{z}$$

But

$$\nabla \times H = \epsilon \frac{\partial E}{\partial t}$$

Comparing these two equations

$$- \frac{\partial H_z}{\partial x} \vec{y} + \frac{\partial H_y}{\partial x} \vec{z} = \epsilon \left[ \frac{\partial E_y}{\partial t} \vec{y} + \frac{\partial E_z}{\partial t} \vec{z} \right]$$

$$[\because E_x = 0]$$

Equating  $\vec{y}$  &  $\vec{z}$  terms

$$- \frac{\partial H_z}{\partial x} = \epsilon \frac{\partial E_y}{\partial t}$$

$$\frac{\partial H_y}{\partial x} = \epsilon \frac{\partial E_z}{\partial t}$$

From Second Maxwell's equation  
for free space

$$\nabla \times E = -\mu \frac{\partial H}{\partial t}$$

But

$$\nabla \times \underline{E} = -\frac{\partial E_z}{\partial x} \vec{y} + \frac{\partial E_y}{\partial x} \vec{z}$$

Equating these two equations

$$-\frac{\partial E_z}{\partial x} \vec{y} + \frac{\partial E_y}{\partial x} \vec{z}$$

$$= -\mu \left[ \frac{\partial H_y}{\partial t} \vec{y} + \frac{\partial H_z}{\partial t} \vec{z} \right]$$

$$[\because H_x = 0]$$

Equating  $\vec{y}$  and  $\vec{z}$  terms

$$\frac{\partial E_z}{\partial x} = \mu \frac{\partial H_y}{\partial t}$$

$$\frac{\partial E_y}{\partial x} = -\mu \frac{\partial H_z}{\partial t}$$

Let the solution for this equation is

$$E_y = [f(x - v_0 t)]$$

Differentiate

$$\frac{\partial E_y}{\partial t} = \frac{\partial f}{\partial (x - v_0 t)} \cdot \frac{\partial (x - v_0 t)}{\partial t}$$

$$= f'(x - v_0 t) (-v_0)$$

Simplify  $f'(x - v_0 t)$  can be written as  $f'$

$$\frac{\partial E_y}{\partial t} = -v_0 f'$$

But

$$-\frac{\partial H_z}{\partial x} = \epsilon \frac{\partial E_y}{\partial t}$$

$$\frac{\partial H_z}{\partial x} = -\epsilon (-v_0 f)'$$

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$$= v_0 \epsilon f'$$

$$= \frac{1}{\sqrt{\mu \epsilon}} \epsilon f'$$

$$\frac{\partial H_z}{\partial x} = \sqrt{\frac{\epsilon}{\mu}} f'$$

Integrating  $H_z = \sqrt{\frac{\epsilon}{\mu}} \int f' dx$

$$H_z = \sqrt{\frac{\epsilon}{\mu}} f$$

$$= \sqrt{\frac{\epsilon}{\mu}} E_y$$



$$\frac{E_y}{H_z} = \sqrt{\frac{\mu}{\epsilon}}$$

Similarly it can be shown that

$$\frac{E_z}{H_y} = -\sqrt{\frac{\mu}{\epsilon}}$$

If  $E$  is the total electric field

$$E = \sqrt{E_y^2 + E_z^2}$$

& Total magnetic field

$$H = \sqrt{H_y^2 + H_z^2}$$

Then

$$\frac{E}{H} = \sqrt{\frac{\mu}{\epsilon}} \quad \text{--- characteristic impedance.}$$

$$\eta = \frac{E}{H} = \sqrt{\frac{\mu}{\epsilon}}$$

For free space  $\epsilon_r = \mu_r = 1$ , then

$$\text{Intrinsic Impedance } \eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi = 377\Omega$$

$$[E \cdot H = 0]$$

5.4.

Wave propagation in Lossless Medium

→ wave equation for free space (lossless medium) is

$$\nabla^2 E = \mu \epsilon \frac{\partial^2 E}{\partial t^2}$$

→ phasor value of  $E$  is

$$E(x, t) = \text{Re} [ (E(x) e^{j\omega t}) ]$$

Applying to wave equation

$$\nabla^2 \text{Re} (E e^{j\omega t}) = \mu \epsilon \frac{\partial^2}{\partial t^2} \text{Re} [E e^{j\omega t}]$$

$$\nabla^2 \text{Re} [E e^{j\omega t}] = \mu \epsilon [-\omega^2 E e^{j\omega t}]$$

$$\text{Re} [ (\nabla^2 E + \mu \epsilon \omega^2 E) e^{j\omega t} ] = 0.$$

$$\nabla^2 E + \mu \epsilon \omega^2 E = 0.$$

This is Vector Helmholtz equation

$$\nabla^2 E + \beta^2 E = 0$$

$$\text{where } \beta^2 = \mu \epsilon \omega^2$$

$$\beta = \sqrt{\mu \epsilon} \omega \quad (\text{phase shift constant})$$

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Wave propagation in  $x$ -direction

is no variation in  $y$  &  $z$

$$\frac{\partial^2 E}{\partial x^2} + \beta^2 E = 0$$

Solution of the equation is

$$E = C_1 e^{-j\beta x} + C_2 e^{j\beta x}$$

5.5. Wave propagation in a Conducting Medium:-

Wave equation for conducting medium  
is

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$$\nabla^2 E - \mu \epsilon \frac{\partial^2 E}{\partial t^2} - \mu \sigma \frac{\partial E}{\partial t} = 0$$

In phasor form

$$\nabla^2 E - \mu \epsilon \omega^2 E - j\omega \sigma \mu E = 0$$

$$\nabla^2 E - j\omega \mu (\sigma + j\omega \epsilon) E = 0.$$

$$\nabla^2 E - \gamma^2 E = 0.$$

$$\gamma^2 = j\omega \mu (\sigma + j\omega \epsilon) \rightarrow \text{propagation constant.}$$



$$\gamma = \alpha + j\beta \longrightarrow \text{phase shift.}$$

↓  
attenuation constant

$$\gamma = \alpha + j\beta$$

$$= \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$$

Squaring both sides

$$\alpha^2 - \beta^2 + 2j\alpha\beta = j\omega\mu\sigma - \omega^2\mu\epsilon$$

Equating real & imaginary parts

$$\alpha^2 - \beta^2 = -\omega^2\mu\epsilon$$

$$\text{and } 2\alpha\beta = \omega\mu\sigma$$

To solve equations

we know that

$$\alpha^2 + \beta^2 = \sqrt{(\alpha^2 - \beta^2)^2 + 4\alpha^2\beta^2}$$

But

$$(\alpha^2 - \beta^2)^2 = (-\omega^2\mu\epsilon)^2$$

$$(2\alpha\beta)^2 = (\omega\mu\sigma)^2$$

$$(\alpha^2 + \beta^2) = \sqrt{\omega^4 \mu^2 \epsilon^2 + \omega^2 \mu^2 \sigma^2}$$

$$\alpha^2 - \beta^2 = -\omega^2 \mu \epsilon$$

Adding two equations

$$2\alpha^2 = -\omega^2 \mu \epsilon + \sqrt{\omega^4 \mu^2 \epsilon^2 + \omega^2 \mu^2 \sigma^2}$$

$$\alpha^2 = \frac{-\omega^2 \mu \epsilon}{2} + \frac{\omega^2 \mu \epsilon}{2} \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}}$$

Attenuation factor is given by

$$\alpha = \omega \sqrt{\frac{\mu \epsilon}{2} \left[ \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} - 1 \right]}$$

then

$$\beta = \omega \sqrt{\frac{\mu \epsilon}{2} \left[ \sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon^2}} + 1 \right]}$$

5.6.

## Skin Depth:-

- In a good conductor, the wave is attenuated as it progresses.
- A new depth of penetration is introduced to explain this situation.
- depth of penetration ( $\delta$ ) is defined as that depth in which the wave has been attenuated to  $1/e$  or 37 percent of its original value.

Amplitude of the wave decreases by the factor  $e^{-\alpha x}$  as it propagates through a distance  $x$

By definition

$$e^{-\alpha x} = \frac{1}{e}$$

$$e^{-\alpha \delta} = e^{-1}$$

$$\alpha \delta = 1$$

$$\delta = \frac{1}{\alpha} \quad (\text{skin depth})$$



5.7.

## Poynting Vector

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### Poynting theorem :-

→ when an electromagnetic wave propagates through space from their source to distant receiving points, there is a transfer of energy from the source to the receivers.

→ There exists a direct relation b/w rate of this energy transfer & amplitude of  $E$  &  $H$  of electromagnetic wave.

Statement :-

Vector product of electric field intensity & magnetic field intensity at any point is a measure of rate of energy flow per unit area at that point.

$$\vec{P} = \vec{E} \times \vec{H}$$

$$\int_V \mathbf{E} \cdot \mathbf{J} dv = - \frac{d}{dt} \int_V \left( \frac{\mu}{2} \mathbf{H}^2 + \frac{\epsilon}{2} \mathbf{E}^2 \right) dv$$

$$= - \oint_S \mathbf{E} \times \mathbf{H} \cdot d\mathbf{s}$$

physical interpretation is

Rate of energy dissipation } = Rate at which stored energy in Volume  $V$  is decreasing

+

Rate at which energy is entering the Volume from outside.

## 5.8 POYNTING VECTOR:-

Vector product of electric field intensity & magnetic field Intensity is another product called Poynting Vector (P)

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Instantaneous, Avg, & Complex Vector:-

$$v = \text{Re} [V e^{j\omega t}] = |V| \cos(\omega t + \theta_v)$$

$$i = \text{Re} [I e^{j\omega t}] = |I| \cos(\omega t + \theta_i)$$

Instantaneous power

$$w = |V| |I| \cos(\omega t + \theta_v) \cos(\omega t + \theta_i)$$

$$w = \frac{|V| |I|}{2} [\cos(\theta_v - \theta_i) + \cos(2\omega t + \theta_v + \theta_i)]$$

Avg power

$$W_{av} = \frac{|V| |I|}{2} \cos(\theta_v - \theta_i)$$

if  $\theta_v - \theta_i = \theta$  angle b/w Voltage & Current then

$$W_{av} = \frac{|V| |I|}{2} \cos \theta.$$

Reactive power

$$W_{avr} = \frac{|V| |I|}{2} \sin \theta.$$



Complex power EnggTree.com

$W$  is defined as

$$W = \frac{1}{2} VI^*$$

$I^*$   $\rightarrow$  Complex conjugate of  $I$ .

$$W = \frac{|V||I|}{2} e^{j\theta}$$

$$W = W_{av} + j W_{ave}$$

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The complex Poynting vector  $P$

$$\hat{n} P = \frac{1}{2} E \times H^*$$

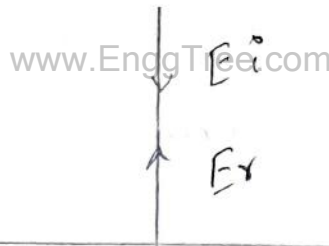
## 5.9. Reflection & Refraction of plane waves:-

(i) Reflection by perfect conductor:-

1. Wave Incident on perfect conductor.

→ when a plane wavefront is incident upon the surface of a perfect conductor - entire wave is reflected.

→ Since no loss within a perfect conductor.



→ resultant Amplitude differs by  $\pi$   
ie  $E_i = -E_r$ .

→ Let electric field incident is  $E_i e^{rx}$ , since  $\alpha = 0$ ,  $r = j\beta$ .

→ Incident wave is  $E_i e^{-j\beta x}$

→ reflected wave is  $E_r e^{j\beta x}$  (opposite)

$$E_T(x) = E_i e^{-j\beta x} + E_r e^{j\beta x}$$

$$E_T(x) = E_i \left[ e^{j\beta x} - e^{-j\beta x} \right]$$

$$= -j 2 E_i \sin \beta x$$

Express the above equation in  
time variation

$$E_T(x, t) = -2j E_i \sin \beta x e^{j\omega t}$$

If  $E_i$  is real

$$E_T(x, t) = +2 E_i \sin \beta x \sin \omega t.$$

This equation shows both waves  
combine to form a standing wave.

|| for magnetic field

$$H_T(x, t) = 2 H_i \cos \beta x \cos \omega t.$$

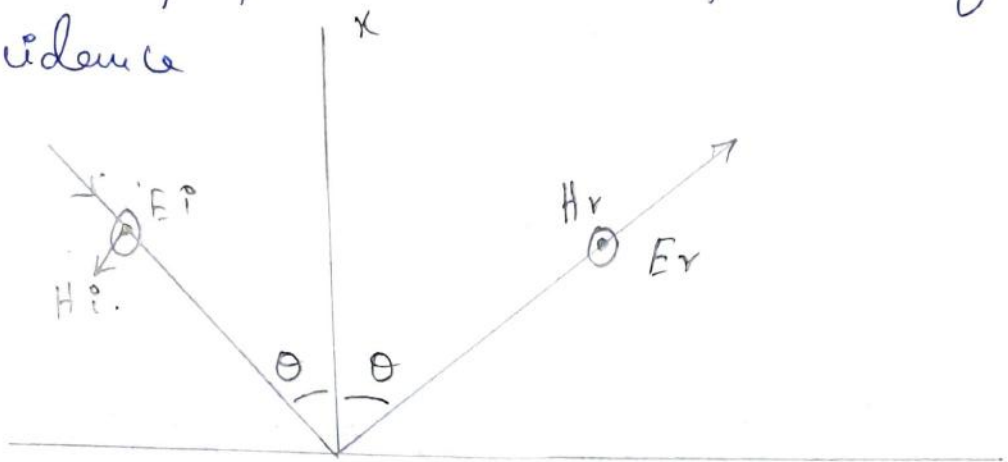
2. wave Incident obliquely on a  
perfect conductor.

→ Two cases arise an oblique condition  
of wave



## Horizontal polarization :-

→  $E$  is perpendicular to the plane of incidence



→ Incident wave can be expressed as

$$E_{in} = E_i e^{-j\beta \bar{n} \cdot \mathbf{r}}$$

→ for normal of incident wave

$$\bar{n} \cdot \mathbf{r} = x \cos \frac{\pi}{2} + y \cos(\frac{\pi}{2} - \theta)$$

$$+ z \cos(\pi - \theta)$$

$$= y \sin \theta - z \cos \theta$$

$$E_{in} = E_i e^{-j\beta(y \sin \theta - z \cos \theta)}$$

||<sup>y</sup> reflected wave

$$E_{ref} = E_r e^{-j\beta(y \sin \theta + z \cos \theta)}$$

But  $E_{ref} = -E_i$

Total electric field

$$E_{\Sigma} = E_{ip} + E_{ref}$$

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$$= E_i \left[ e^{-j\beta(y \sin\theta - z \cos\theta)} - e^{-j\beta(y \sin\theta + z \cos\theta)} \right]$$

$$= 2j E_i \sin(\beta z \cos\theta) e^{-j\beta y \sin\theta}$$

$$E_T = 2j E_i \sin\beta_z z e^{-j\beta y y}$$

where  $\beta = \frac{\omega}{v} = \frac{2\pi f}{v} = \frac{2\pi}{\lambda}$

$$\beta_x = \beta \cos\theta$$

$$\beta_y = \beta \sin\theta$$

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Wave length in z-direction

$$\lambda_z = \frac{2\pi}{\beta_x} = \frac{\lambda}{\cos\theta}$$

Velocity in y direction

$$V_y = \frac{\omega}{\beta_y} = \frac{v}{\sin\theta}$$

$$\lambda_y = \frac{\lambda}{\sin\theta}$$

Vertical polarization:-

→  $E \parallel$  to plane of incidence.

→  $H_i$  &  $H_r$  makes angle  $\theta_i = \theta_r = \theta$ .

→ incident wave is expressed as

$$H_{in} = H_i e^{-j\beta(y \sin \theta - z \cos \theta)}$$

→ reflected wave as

$$H_{ref} = H_r e^{-j\beta(y \sin \theta + z \cos \theta)}$$

$$H_T = H_{in} + H_{ref} \quad (\text{no phase reversal})$$

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$$H_T = H_i e^{j\beta y \sin \theta} \left[ e^{-j\beta z \cos \theta} + e^{-j\beta z \cos \theta} \right]$$

$$H_T = 2 H_i \cos \beta_z z e^{-j\beta y y}$$

(ii) Reflection by a perfect Dielectric

1) wave incident normally on a

perfect dielectric:-

→ consider two perfect dielectric media

→ let  $\epsilon_1, \mu_1$  &  $\epsilon_2, \mu_2$  be permittivity &

permeability of medium 1 & 2.



$$E_i = \eta_1 H_i^o$$

$$E_r = -\eta_1 H_r$$

$$E_t = \eta_2 H_t.$$

According to boundary condition,  
tangential component of  $E$  or  $H$   
is continuous

$$H_i + H_r = H_t$$

$$\& \quad E_i + E_r = E_t.$$

From above equations

$$H_i = \frac{E_i}{\eta_1}, \quad H_r = -\frac{E_r}{\eta_1} \text{ and}$$

$$H_t = \frac{E_t}{\eta_2}$$

$$H_t = H_i + H_r = \frac{1}{\eta_1} [E_i - E_r]$$

$$H_t = \frac{E_t}{\eta_2}$$

$$H_t = \frac{1}{\eta_2} [E_i + E_r]$$

Equating  $H_t$  becomes EnggTree.com

$$\frac{1}{\eta_1} [E_i - E_r] = \frac{1}{\eta_2} [E_i + E_r]$$

$$\eta_2 [E_i - E_r] = \eta_1 [E_i + E_r]$$

$$E_i [\eta_2 - \eta_1] = E_r [\eta_1 + \eta_2]$$

Reflection Co-efficient

$$\frac{E_r}{E_i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

also

$$\begin{aligned} \frac{E_t}{E_i} &= \frac{E_i + E_r}{E_i} = 1 + \frac{E_r}{E_i} \\ &= 1 + \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \end{aligned}$$

Transmission Co-efficient }  $\frac{E_t}{E_i} = \frac{2\eta_2}{\eta_1 + \eta_2}$

114 for magnetic field

$$\frac{H_r}{H_i} = \frac{\eta_1 - \eta_2}{\eta_2 + \eta_1} \quad \&$$

$$\frac{H_t}{H_i} = \frac{2\eta_1}{\eta_1 + \eta_2}$$

In terms of permittivity

$$\frac{E_r}{E_i} = \frac{\sqrt{\epsilon_1} - \sqrt{\epsilon_2}}{\sqrt{\epsilon_1} + \sqrt{\epsilon_2}} \quad \text{and}$$

$$\frac{E_t}{E_i} = \frac{2\sqrt{\epsilon_1}}{\sqrt{\epsilon_1} + \sqrt{\epsilon_2}}$$

114 for magnetic field.

2) Oblique wave incident.

$$\frac{E_r^2}{E_i^2} = 1 - \frac{\sqrt{\epsilon_2} E_t^2 \cos \theta_t}{\sqrt{\epsilon_1} E_i^2 \cos \theta_i} \quad \&$$

$$\frac{E_r}{E_i} = \frac{\cos \theta_i - \sqrt{\frac{\epsilon_2}{\epsilon_1} \sin^2 \theta_i}}{\cos \theta_i + \sqrt{\frac{\epsilon_2}{\epsilon_1} \sin^2 \theta_i}}$$

Brewster's angle:-

$$\tan \theta_i = \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

at which no reflected wave is polarized.



UNIT - I

Q 1. Given two Vectors  $\vec{A} = 3\vec{a}_x - \vec{a}_y + 8\vec{a}_z$   
and  $\vec{B} = 2\vec{a}_x + 3\vec{a}_y - \vec{a}_z$ . Find the  
dot product & Angle b/w them.

Given :-

$$\vec{A} = 3\vec{a}_x - \vec{a}_y + 8\vec{a}_z$$

$$\vec{B} = 2\vec{a}_x + 3\vec{a}_y - \vec{a}_z$$

$$\vec{A} \cdot \vec{B} = (3\vec{a}_x - \vec{a}_y + 8\vec{a}_z) \cdot (2\vec{a}_x + 3\vec{a}_y - \vec{a}_z)$$

$$= (3)(2) + (-1)(3) + (8)(-1)$$

$$= 6 - 3 - 8$$

$$\vec{A} \cdot \vec{B} = \underline{\underline{-5}}$$

$$|\vec{A}| = \sqrt{(3)^2 + (-1)^2 + (8)^2} = \sqrt{74}$$

$$|\vec{B}| = \sqrt{(2)^2 + 3^2 + (-1)^2} = \sqrt{14}$$

$$\theta = \cos^{-1} \left[ \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|} \right] = \cos^{-1} \left[ \frac{-5}{\sqrt{74} \sqrt{14}} \right]$$

$$\theta = 98.92^\circ$$

Q 2. Given two Vectors  $\vec{A} = \vec{a}_x - 5\vec{a}_y + 2\vec{a}_z$  and  $\vec{B} = 3\vec{a}_x - \vec{a}_y - 4\vec{a}_z$ . Find the Cross product and unit normal Vector.

Given :

$$\vec{A} = \vec{a}_x - 5\vec{a}_y + 2\vec{a}_z$$

$$\vec{B} = 3\vec{a}_x - \vec{a}_y - 4\vec{a}_z$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ 1 & -5 & 2 \\ 3 & -1 & -4 \end{vmatrix}$$

$$= \vec{a}_x (20+2) - \vec{a}_y (-4-6) + \vec{a}_z (-1+15)$$

$$\vec{A} \times \vec{B} = 22\vec{a}_x + 10\vec{a}_y + 14\vec{a}_z$$

$$|\vec{A} \times \vec{B}| = \sqrt{484 + 100 + 196} = \sqrt{780}$$

$\vec{a}_n \rightarrow$  unit Vector

$$\vec{a}_n = \frac{\vec{A} \times \vec{B}}{|\vec{A} \times \vec{B}|}$$

$$= \frac{1}{\sqrt{780}} (22\vec{a}_x + 10\vec{a}_y + 14\vec{a}_z)$$

Q3. Give the cylindrical coordinates of the point whose Cartesian coordinates are  $x=2$ ,  $y=4$  &  $z=5$  units.

Sol: Given  $x=2$ ,  $y=4$ ,  $z=5$

$$\rho = \sqrt{x^2 + y^2} = \sqrt{4 + 16} = \sqrt{20} = 2\sqrt{5}$$

$$\phi = \tan^{-1}(y/x) = \tan^{-1}(4/2) = 53.13^\circ$$

$$z = z = \underline{\underline{5}}$$

The cylindrical coordinates are

$$(\rho, \phi, z) = (2\sqrt{5}, 53.13, 5)$$

Q4. Give the Cartesian coordinates of the point whose cylindrical coordinates are  $\rho=2$ ,  $\phi=45^\circ$  and  $z=-1$

Sol:

$$x = \rho \cos \phi \quad y = \rho \sin \phi \quad z = z$$

$$x = 2 \cos 45^\circ$$

$$y = 2 \sin 45^\circ \quad z = -1$$

$$x = \underline{\underline{0.707}}$$

$$y = \underline{\underline{0.707}} \quad z = \underline{\underline{-1}}$$

Cartesian coordinates are  $(x, y, z) =$

$$(\underline{\underline{0.707}}, \underline{\underline{0.707}}, \underline{\underline{-1}})$$



Q 5. Give the spherical coordinates of the point whose Cartesian coordinates are

$$x = -1, y = 2 \text{ and } z = 5$$

Sol:

$$r = \sqrt{x^2 + y^2 + z^2}$$

$$= \sqrt{1 + 4 + 25}$$

$$= \sqrt{30} //$$

$$\phi = \tan^{-1}(y/x)$$

$$= \tan^{-1}(2/-1)$$

$$= \tan^{-1}(-2)$$

$$\theta = \cos^{-1}\left(\frac{z}{\sqrt{x^2 + y^2 + z^2}}\right)$$

$$= \cos^{-1}\left(\frac{5}{\sqrt{30}}\right) //$$

Spherical coordinates are

$$(r, \phi, \theta).$$

Q 6. Given points  $A(x=2, y=2, z=-1)$

$B(\rho=4, \phi=50^\circ, z=2)$ . Find the distance from A to B.

Given.  $A(x=2, y=2, z=-1)$

$B(\rho=4, \phi=-50^\circ, z=2)$

$$x = \rho \cos \phi \qquad y = \rho \sin \phi$$
$$= 4 \cos(-50^\circ) \qquad = 4 \sin(-50^\circ)$$

$$x = \underline{\underline{2.571}} \qquad y = \underline{\underline{-3.064}}$$

$$\boxed{z = z = 2}$$

So distance from A to B.

$$= \sqrt{(2.571-2)^2 + (-3.064-2)^2 + (2+1)^2}$$

$$= \sqrt{46.098}$$

$$d = \underline{\underline{6.789}}$$

Q7. The scalar fields are given by,

$$(i) \quad V = 20 e^{-x} \sin(\pi/b)y.$$

$$(ii) \quad V = 25 \rho \sin \phi$$

$$(iii) \quad V = \frac{40 \cos \theta}{r^2}$$

Find its gradient at the point  $(P(0,1,1))$   
 for Cartesian,  $P(\sqrt{2}, \pi/2, 5)$  for  
 cylindrical,  $P(3, 60^\circ, 30^\circ)$  for spherical.

Given :

$$V = 20 e^{-x} \sin(\pi/b)y$$

$$\nabla V = \frac{\partial V}{\partial x} \vec{a}_x + \frac{\partial V}{\partial y} \vec{a}_y + \frac{\partial V}{\partial z} \vec{a}_z$$

$$\frac{\partial V}{\partial x} = -20 e^{-x} \sin(\pi/b)y$$

$$\frac{\partial V}{\partial y} = 20 e^{-x} \frac{\pi}{b} \cos(\pi/b)y.$$

$$\frac{\partial V}{\partial z} = 0.$$

$$\nabla V|_{P(0,1,1)} = [-20 \sin \pi/6] \vec{a}_x + [20 \times \pi/6 \times \cos \pi/6] \vec{a}_y$$

$$\nabla V = -10 \vec{a}_x + 9.07 \vec{a}_y //$$



For cylindrical:-

$$\frac{\partial V}{\partial \rho} = 25 \sin \phi$$

$$\frac{\partial V}{\partial \phi} = 25 \rho \cos \phi$$

$$\frac{\partial V}{\partial z} = 0.$$

$$\nabla V = [25 \sin \phi] \vec{a}_\rho + \frac{1}{\rho} [25 \rho \cos \phi] \vec{a}_\phi$$

$$\nabla V \Big|_{(\sqrt{2}, \pi/2, 5)}$$

$$= [25 \sin \pi/2] \vec{a}_\rho + [25 \cos \pi/2] \vec{a}_\phi$$

$$\nabla V \Big|_{(\sqrt{2}, \pi/2, 5)} = 25 \vec{a}_\rho$$

For spherical

$$\nabla V = \frac{\partial V}{\partial r} \vec{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \vec{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \vec{a}_\phi$$

$$\frac{\partial V}{\partial r} = \frac{-80 \cos \theta}{r^3}$$

$$\frac{\partial V}{\partial \phi} = 0.$$

$$\frac{\partial V}{\partial \theta} = -40 \sin \theta$$

$$\nabla V / (3, 60, 30) \\ = \left[ \frac{-80 \cos 60^\circ}{27} \right] \vec{a}_r - \left[ \frac{40 \sin 60^\circ}{27} \right] \vec{a}_\phi$$

$$\nabla V = -1.48 \vec{a}_r - 1.28 \vec{a}_\phi$$

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Q. 8. Determine the divergence of the Vector field.

$$(i) \vec{P} = x^2 y z \vec{a}_x + x z \vec{a}_z$$

$$(ii) \vec{Q} = \rho \sin \phi \vec{a}_\rho + \rho^2 z \vec{a}_\phi + z \cos \phi \vec{a}_z$$

$$(iii) \vec{r} = \frac{1}{r^2} (\cos \theta \vec{a}_r + r \sin \theta \cos \phi \vec{a}_\phi + r \sin \theta \sin \phi \vec{a}_\phi)$$

Solution:-

Cartesian

$$\nabla \cdot \vec{P} = \frac{\partial P_x}{\partial x} + \frac{\partial P_y}{\partial y} + \frac{\partial P_z}{\partial z}$$

$$P_x = x^2 y z, P_y = 0, P_z = x z.$$

$$\nabla \cdot \vec{P} = \frac{\partial (x^2 y z)}{\partial x} + \frac{\partial (0)}{\partial y} + \frac{\partial (x z)}{\partial z}$$

$$= 2x y z + x$$

For cylindrical :-

$$\nabla \cdot \vec{Q} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho Q_\rho) + \frac{1}{\rho} \frac{\partial Q_\phi}{\partial \phi} + \frac{\partial Q_z}{\partial z}$$

Given

$$Q_\rho = \rho \sin \phi, \quad Q_\phi = \rho^2 z$$

$$Q_z = z \cos \phi.$$

$$\nabla \cdot \vec{Q} = \frac{1}{\rho} (2\rho \sin \phi) + \frac{1}{\rho} (0) + \cos \phi.$$

$$\nabla \cdot \vec{Q} = 2 \sin \phi + \cos \phi$$

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For spherical :-

$$\nabla \cdot \vec{T} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 T_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (T_\theta \sin \theta)$$

$$+ \frac{1}{r \sin \theta} \frac{\partial T_\phi}{\partial \phi}.$$

$$T_r = \frac{1}{r^2} \cos \theta, \quad T_\theta = r \sin \theta \cos \phi, \quad T_\phi = \cos \theta$$

$$\nabla \cdot \vec{T} = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \times \frac{1}{r^2} \cos \theta \right) + \frac{1}{r \sin \theta} \left[ \right.$$

$$\left. r \sin^2 \theta \cos \phi \right] + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} (\cos \theta)$$

$$= \frac{\cos \phi}{\sin \theta} \left( \frac{2 \sin 2\theta}{2} \right) = \frac{\cos \phi}{\sin \theta} \times 2 \sin \theta \cos \theta$$

$$\nabla \cdot \vec{T} = 2 \cos \theta \cos \phi.$$



Q9.

The Vector field  $\vec{D} = \frac{5r^2}{4} \vec{a}_r$  is given in Spherical Coordinate System. Evaluate both Sides of divergence Theorem for the Volume enclosed between

(i)  $r=1$  and  $r=2$

(ii)  $\theta=0$  to  $\pi/4$  and  $r=4$ .

Sol:

Case(i) :-  $r=1$  &  $r=2$ .

By divergence Theorem

$$\iiint_V (\nabla \cdot \vec{D}) dV = \iint_S \vec{D} \cdot d\vec{s}$$

LHS

$$\iiint_V (\nabla \cdot \vec{D}) dV.$$

$$\nabla \cdot \vec{D} = \frac{1}{r^2} \frac{d}{dr} \left( r^2 \times \frac{5r^2}{4} \right)$$

$$= \frac{1}{r^2} \times \frac{5}{4} \times 4r^3.$$

$$\nabla \cdot \vec{D} = 5r. \quad 2\pi \quad r=2$$

$$\iiint_V (\nabla \cdot \vec{D}) dV = \int \int \int 5r \times r^2 \sin \theta \, dr \, d\theta \, d\phi$$

$\phi=0$   $\theta=0$   $r=1$

$$\begin{aligned}
 &= 5 \int_0^{2\pi} \int_0^{\pi} \int_{r=1}^2 r^3 \sin\theta \, dr \, d\theta \, d\phi \\
 &= 5 \int_0^{2\pi} \int_0^{\pi} \int_{r=1}^2 \left[ \frac{r^4}{4} \right]_1^2 \sin\theta \, d\theta \, d\phi \\
 &= 5 \frac{(16-1)}{4} \int_0^{2\pi} [-\cos\theta]_0^{\pi} \, d\phi \\
 &= \frac{75}{4} \int_0^{2\pi} (1+1) \, d\phi \\
 &= \frac{75}{2} [\phi]_0^{2\pi} = \frac{75}{2} \times 2\pi = 75\pi
 \end{aligned}$$

①

RHS:

$$\oint \vec{D} \cdot d\vec{s}$$

$$\begin{aligned}
 \iint \vec{D} \cdot d\vec{s} &= \iint_{r=2} \vec{D} \cdot ds \, \vec{a}_r - \iint_{r=1} \vec{D} \cdot ds \, \vec{a}_r \\
 &= \iint \frac{5r^4}{4} \sin\theta \, d\theta \, d\phi - \iint_{r=1} \frac{5r^4}{4} \sin\theta \, d\theta \, d\phi \\
 &= \frac{5(2)^4}{4} \int_0^{2\pi} \int_0^{\pi} \sin\theta \, d\theta \, d\phi - \frac{5(1)^4}{4} \int_0^{2\pi} \int_0^{\pi} \sin\theta \, d\theta \, d\phi
 \end{aligned}$$

$$= 20 \int_0^{2\pi} [-\cos\theta]_0^{2\pi} d\phi - \frac{5}{4} \int_0^{2\pi} [-\cos\theta]_0^{2\pi} d\phi$$

$$= 40 [\phi]_0^{2\pi} - \frac{5}{2} [\phi]_0^{2\pi}$$

$$= 80\pi - 5\pi = 75\pi \quad \text{--- (2)}$$

from equation (1) & (2)

$$\iiint_V \vec{\nabla} \cdot \vec{D} \, dV = \iint \vec{D} \cdot d\vec{s}$$

Case (ii)  $\theta = 0$  to  $\pi/4$  &  $r = 4$ .

$$\text{LHS: } \iiint \nabla \cdot \vec{D} \, dV$$

$$= \int_{\phi=0}^{2\pi} \int_{r=0}^{4} \int_{\theta=0}^{\pi/4} 5r^3 \sin\theta \, dr \, d\theta \, d\phi$$

$$= \frac{5(4)^4}{4} \int_0^{2\pi} [-\cos\theta]_0^{\pi/4} d\phi$$

$$= 320 \int_0^{2\pi} [-\cos\pi/4 + \cos\theta] d\theta$$



$$= 320 \times 0.293 \left[ \phi \right]_0^{2\pi}$$

$$= 320 \times 0.293 \times 2\pi$$

$$\iiint_V \nabla \cdot \vec{D} dv = 187.45\pi \quad \text{--- (1)}$$

RHS  $\iint_S \vec{D} \cdot d\vec{s}$

$$= \iint_{r=4} \vec{D} \cdot d\vec{s} \vec{a}_r + \iint \vec{D} \cdot d\vec{s} \vec{a}_\theta$$

$$= \iint_{r=4} \frac{5r^4}{4} \sin\theta d\theta d\phi + 0.$$

$$= \frac{5(4)^4}{4} \int_0^{2\pi} \int_0^{\pi/4} \sin\theta d\theta d\phi$$

$$= 320 \int_0^{2\pi} \left[ -\cos\theta \right]_0^{\pi/4} d\phi.$$

$$= 320 \times 0.293 \times 2\pi$$

$$\iint_S \vec{D} \cdot d\vec{s} = 187.45\pi \quad \text{--- (2)}$$

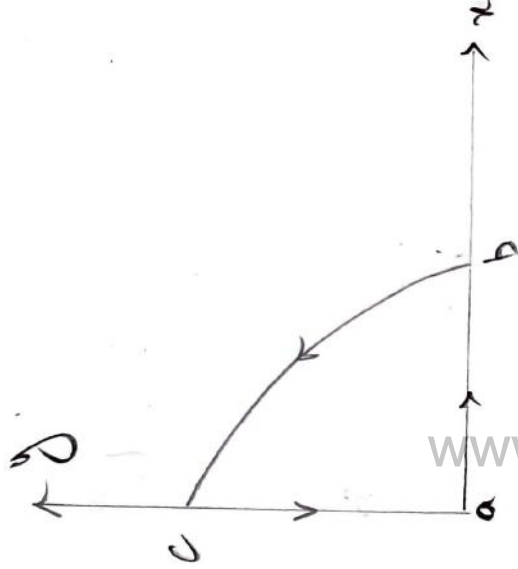
From eq (1) & (2)

Divergence theorem is proved.

Q10. Given  $\vec{A} = 2\rho \cos\phi \vec{a}_\rho + \rho^2 \vec{a}_\phi$  in

Cylindrical coordinate system for contour

Shown in figure. Verify using Stokes' theorem.



Given  $\vec{A} = 2\rho \cos\phi \vec{a}_\rho + \rho^2 \vec{a}_\phi$

By Stokes' theorem

$$\oint_C \vec{A} \cdot d\vec{l} = \iint_S (\nabla \times \vec{A}) \cdot \vec{ds}$$

RHS  $\iint_S (\nabla \times \vec{A}) \cdot \vec{ds}$

$$\nabla \times \vec{A} = \frac{1}{\rho} \begin{vmatrix} \vec{a}_\rho & \rho \vec{a}_\phi & \vec{a}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ 2\rho \cos\phi & \rho^2 & 0 \end{vmatrix}$$

$$= \frac{1}{\rho} \left[ \vec{a}_\rho (0-0) - \rho \vec{a}_\phi (0-0) + \vec{a}_z (2\rho + 2\rho \sin\phi) \right]$$

$$= \frac{1}{\rho} \times \int \int [2 + 2 \sin \phi] \vec{a}_z$$

$$\nabla \times \vec{A} = (2 + 2 \sin \phi) \vec{a}_z$$

$$\therefore d\vec{s} = \rho d\rho d\phi \vec{a}_z$$

$$(\nabla \times \vec{A}) \cdot d\vec{s} = 2(1 + \sin \phi) \rho d\rho d\phi$$

$$\iint_S (\nabla \times \vec{A}) \cdot d\vec{s} = \int_0^{\pi/2} \int_0^{\pi/2} 2(1 + \sin \phi) \rho d\rho d\phi$$

$$= 2 \int_0^{\pi/2} (1 + \sin \phi) \left( \frac{\rho^2}{2} \right)_0^1 d\phi$$

$$= 2 \times \frac{1}{2} [\phi - \cos \phi]_0^{\pi/2}$$

$$= \left( \frac{\pi}{2} - \cos \frac{\pi}{2} \right) - (0 - \cos 0)$$

$$= \left( \frac{\pi}{2} - 0 \right) - (0 - 1)$$

$$= 1 + \frac{\pi}{2} \quad \text{--- (1)}$$

LHS

$$\oint \vec{A} \cdot d\vec{l} = \int_{AB} \vec{A} \cdot d\vec{l} + \int_{BC} \vec{A} \cdot d\vec{l} + \int_{CA} \vec{A} \cdot d\vec{l}$$



For path AB: - EnggTree.com

$$\int_{AB} \vec{A} \cdot d\vec{r} = \int_{\phi=0} 2\rho \cos \phi \, d\rho.$$

$$= 2 \left[ \frac{\rho^2}{2} \right]_0^1 = 2 \left( \frac{1}{2} \right) = 1$$

↳ (A)

For path BC

$$\int_{BC} \vec{A} \cdot d\vec{r} = \int_{\rho=1} \rho^3 \, d\phi = \int_0^{\pi/2} d\phi = \pi/2.$$

↳ (B)

For path CA: - www.EnggTree.com

$$\int_{CA} \vec{A} \cdot d\vec{r} = \int_{\phi=\pi/2} 2\rho \cos \phi \, d\rho$$
$$= \int_0^1 0 = 0 \quad \text{--- (C)}$$

From (A), (B), (C)

$$\oint \vec{A} \cdot d\vec{r} = 1 + \pi/2 \quad \text{--- (2)}$$

From eq (1) & (2)

Stokes theorem is verified.

Q11. Find the force of interaction between two charges spaced 10cm apart in vacuum. The charges are  $4 \times 10^{-8} \text{ C}$  and  $6 \times 10^{-5} \text{ C}$ . If the same charges separated by the same distance in kerosene ( $\epsilon_r = 2$ ), what is the force of interaction between them?

Sol:

$$Q_1 = 4 \times 10^{-8} \text{ C} \quad \epsilon_r = 1$$

$$Q_2 = 6 \times 10^{-5} \text{ C} \quad \epsilon_r = 2$$

$$r = 10 \text{ cm} = 10 \times 10^{-2} \text{ m} = 0.1 \text{ m}$$

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For Vacuum

$$F = \frac{Q_1 Q_2}{4\pi \epsilon_0 \epsilon_r r^2} = \frac{4 \times 10^{-8} \times 6 \times 10^{-5}}{4 \times 3.14 \times 8.854 \times 10^{-12} \times (0.1)^2}$$

$$F = 2.15 \text{ N}$$

for kerosene

$$F = \frac{Q_1 Q_2}{4\pi \epsilon_0 \epsilon_r r^2} = \frac{4 \times 10^{-8} \times 6 \times 10^{-5}}{4 \times 3.14 \times 8.854 \times 10^{-12} \times 2 \times (0.1)^2}$$

$$F = 1.075 \text{ N}$$

Q:12

A point charge of  $10 \mu\text{C}$  is located at  $(1, 2, 3)$  and another point charge of  $-3 \mu\text{C}$  is located at  $(3, 0, 2)$  in vacuum. Find the force b/w them?

Sol:

$$Q_1 = 10 \mu\text{C} = 10 \times 10^{-6} \text{ C}$$

$$Q_2 = -3 \mu\text{C} = -3 \times 10^{-6} \text{ C}$$

$$\vec{r}_1 = \vec{a}_x + 2\vec{a}_y + 3\vec{a}_z$$

$$\vec{r}_2 = 3\vec{a}_x + 2\vec{a}_z$$

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$$\epsilon_r = 1$$

$$\vec{r}_{12} = \vec{r}_2 - \vec{r}_1 = 2\vec{a}_x - 2\vec{a}_y - \vec{a}_z$$

$$r_{12} = |\vec{r}_{12}| = \sqrt{4 + 4 + 1} = 3$$

$$\vec{u}_{12} = \frac{\vec{r}_{12}}{|\vec{r}_{12}|} = \frac{2\vec{a}_x - 2\vec{a}_y - \vec{a}_z}{3}$$

$$\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi \epsilon_0 \epsilon_r r_{12}^2} \vec{u}_{12}$$

$$= \frac{(10 \times 10^{-6})(-3 \times 10^{-6})}{4 \times 3.14 \times 8.854 \times 10^{-12} \times (3)^2} \vec{u}_{12}$$



$$\vec{F}_{12} = -0.02\vec{a}_x + 0.02\vec{a}_y - 0.01\vec{a}_z$$

$$F_{12} = |\vec{F}_{12}| = \underline{\underline{0.03\text{N}}}$$